

# NERC

NORTH AMERICAN ELECTRIC  
RELIABILITY CORPORATION

# Inverter-Based Resource Disturbance Analysis

Key Findings and Recommendations

Informational Webinar  
February 15, 2018

**RELIABILITY | ACCOUNTABILITY**

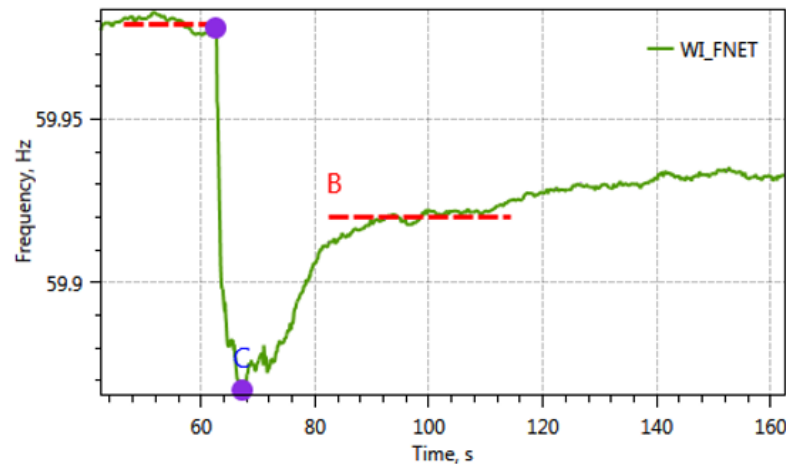
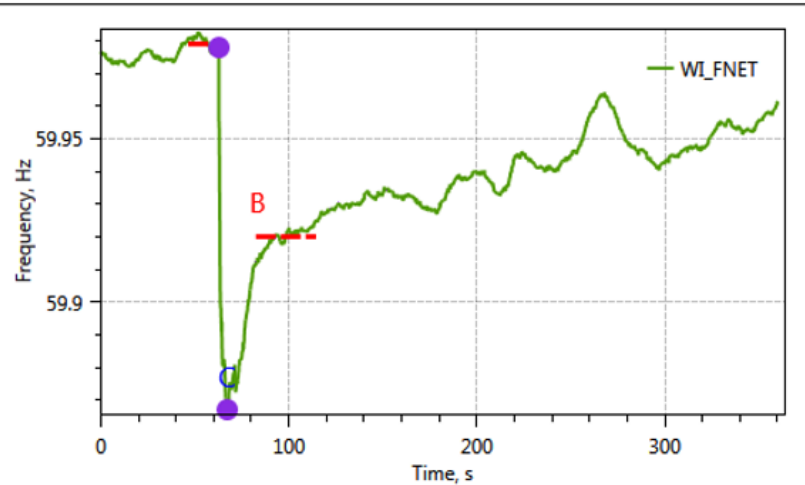


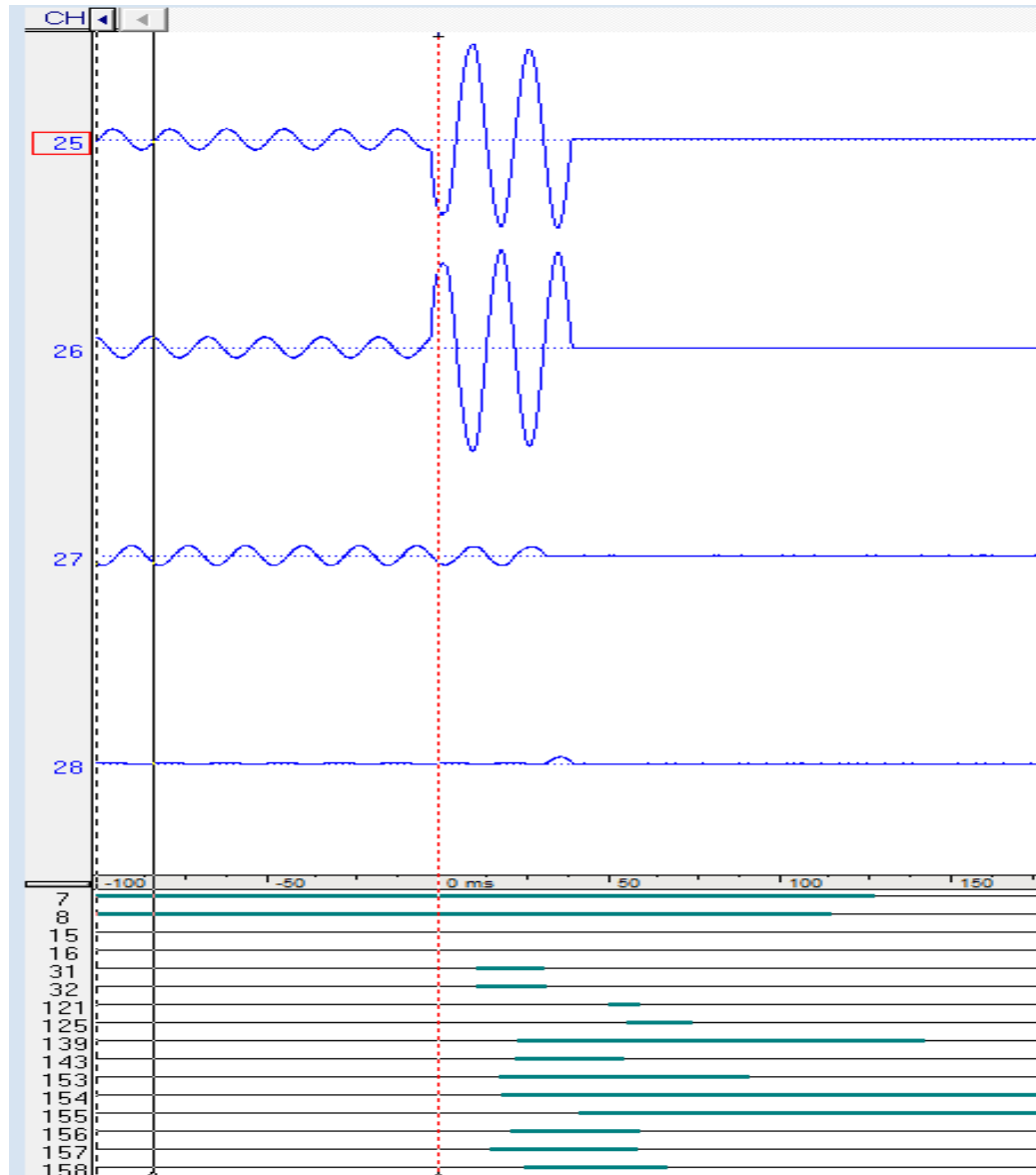
**August 16, 2016**  
**Blue Cut Fire Disturbance**

*Key Findings and Recommendations*

WI\_20160816\_184506

|                   |                     |
|-------------------|---------------------|
| Event ID          | WI_20160816_184506  |
| Event Description | ""                  |
| UTC Time          | 08/16/2016 18:45:06 |
| Local Time        | 08/16/2016 11:45:06 |
| Time Zone         | PDT                 |
| M4 Flag           | Yes                 |
| BAL003 Flag       | Yes                 |
| MW Loss           | 0                   |
| Value A           | 59.979              |
| Value B           | 59.92               |
| Point C           | 59.8669             |
| Time of C         | 4.7                 |
| Point C'          | -                   |
| Time of C'        | -                   |
| A-B [mHz]         | 59                  |
| A-C [mHz]         | 112                 |
| FRM_B [MW/0.1Hz]  | 0                   |
| FRM_C [MW/0.1Hz]  | 0                   |



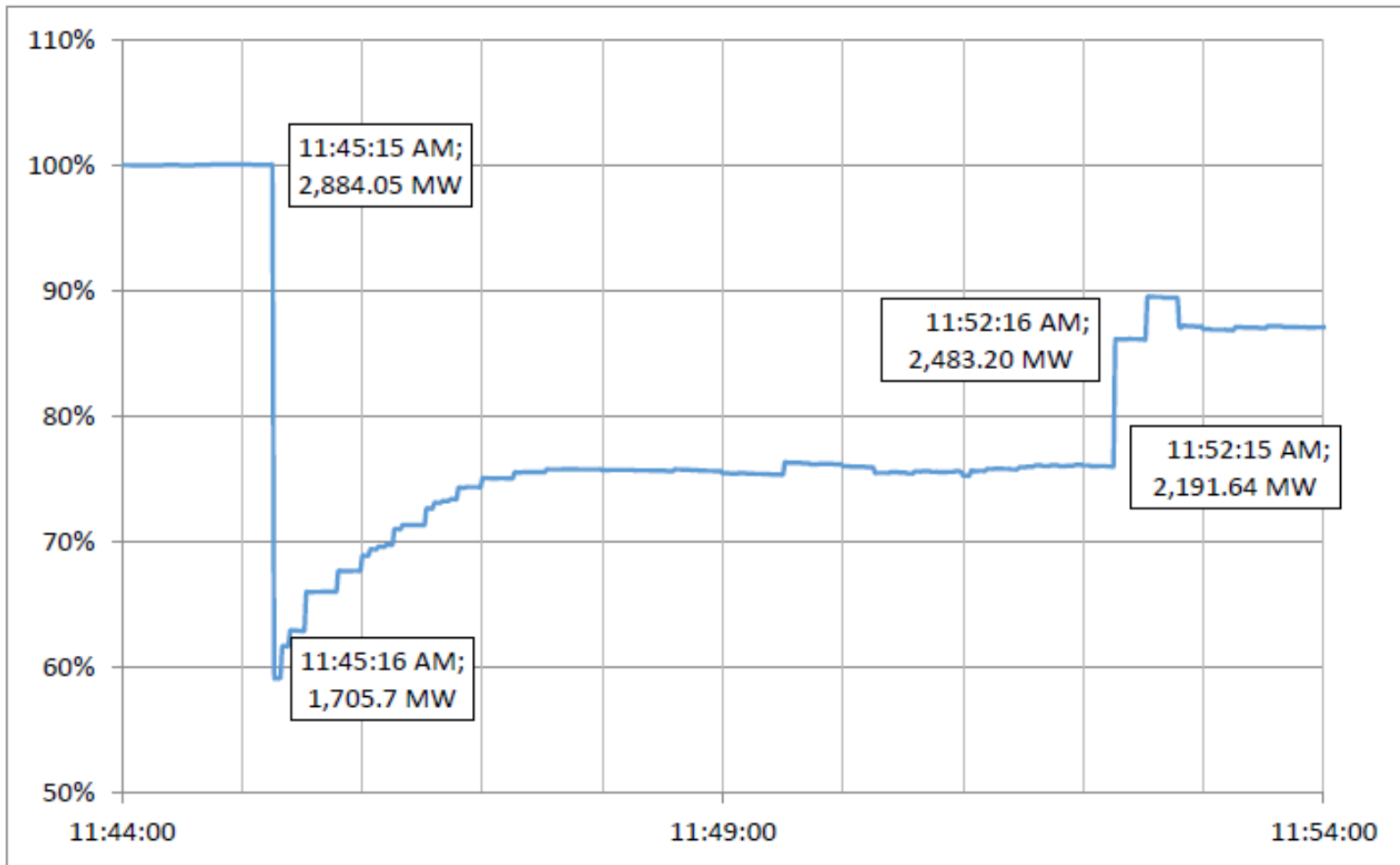


**Phase A amps**

**Phase B amps**

**Phase C amps**

**Residual amps**



- 26 different solar developments
- All utility scale
- Majority connected at 500kV or 230kV
- 10 different inverter manufacturers
- Reported causes of “trips”
  - Under frequency
  - Under voltage
  - Over voltage
  - DC overcurrent
  - 1 loss of synchronism

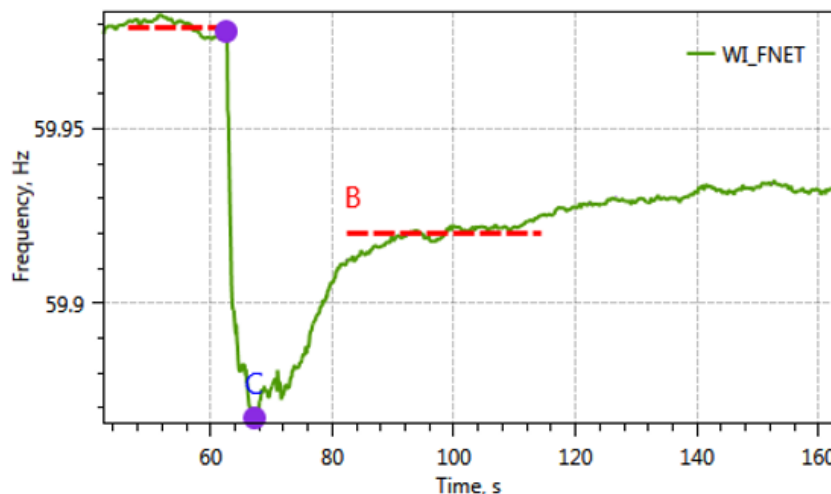
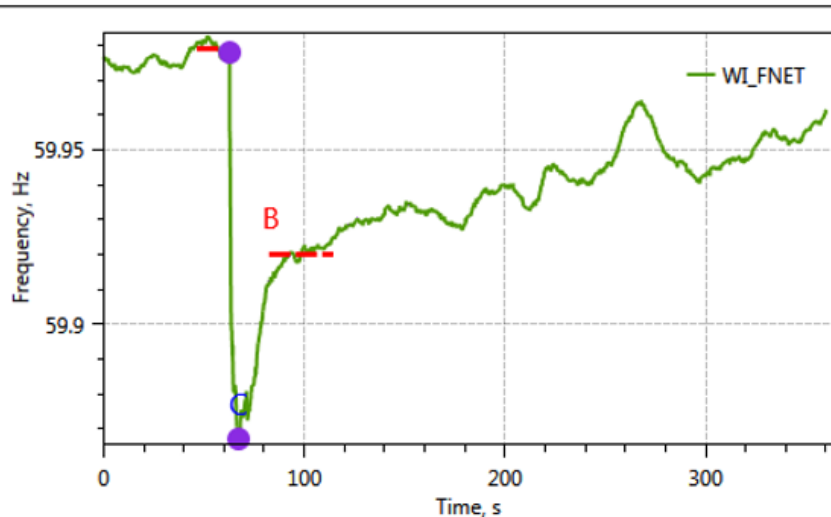
| #  | Date/Time           | Fault Location | Fault Type          | Clearing Time (cycles) | Lost Generation (MW) | Geographic Impact  |
|----|---------------------|----------------|---------------------|------------------------|----------------------|--------------------|
| 1  | 08/16/2016<br>11:45 | 500 kV line    | Line to Line (AB)   | 2.49                   | 1,178                | Widespread         |
| 2  | 08/16/2016<br>14:04 | 500 kV line    | Line to Ground (AG) | 2.93                   | 234                  | Somewhat Localized |
| 3  | 08/16/2016<br>15:13 | 500 kV line    | Line to Ground (AG) | 3.45                   | 311                  | Widespread         |
| 4  | 08/16/2016<br>15:19 | 500 kV line    | Line to Ground (AG) | 3.05                   | 30                   | Localized          |
| 5  | 09/06/2016<br>13:17 | 220 kV line    | Line to Ground (AG) | 2.5                    | 490                  | Localized          |
| 6  | 09/12/2016<br>17:40 | 500 kV line    | Line to Ground (BG) | 3.04                   | 62                   | Localized          |
| 7  | 11/12/2016<br>10:00 | 500 kV CB      | Line to Ground (CG) | 2.05                   | 231                  | Widespread         |
| 8  | 02/06/2017<br>12:13 | 500 kV line    | Line to Ground (BG) | 2.97                   | 319                  | Widespread         |
| 9  | 02/06/2017<br>12:31 | 500 kV line    | Line to Ground (BG) | 3.01                   | 38                   | Localized          |
| 10 | 02/06/2017<br>13:03 | 500 kV line    | Line to Ground (BG) | 3.00                   | 543                  | Widespread         |
| 11 | 05/10/2017<br>10:13 | 500 kV line    | unknown             | unknown                | 579                  | Somewhat Localized |

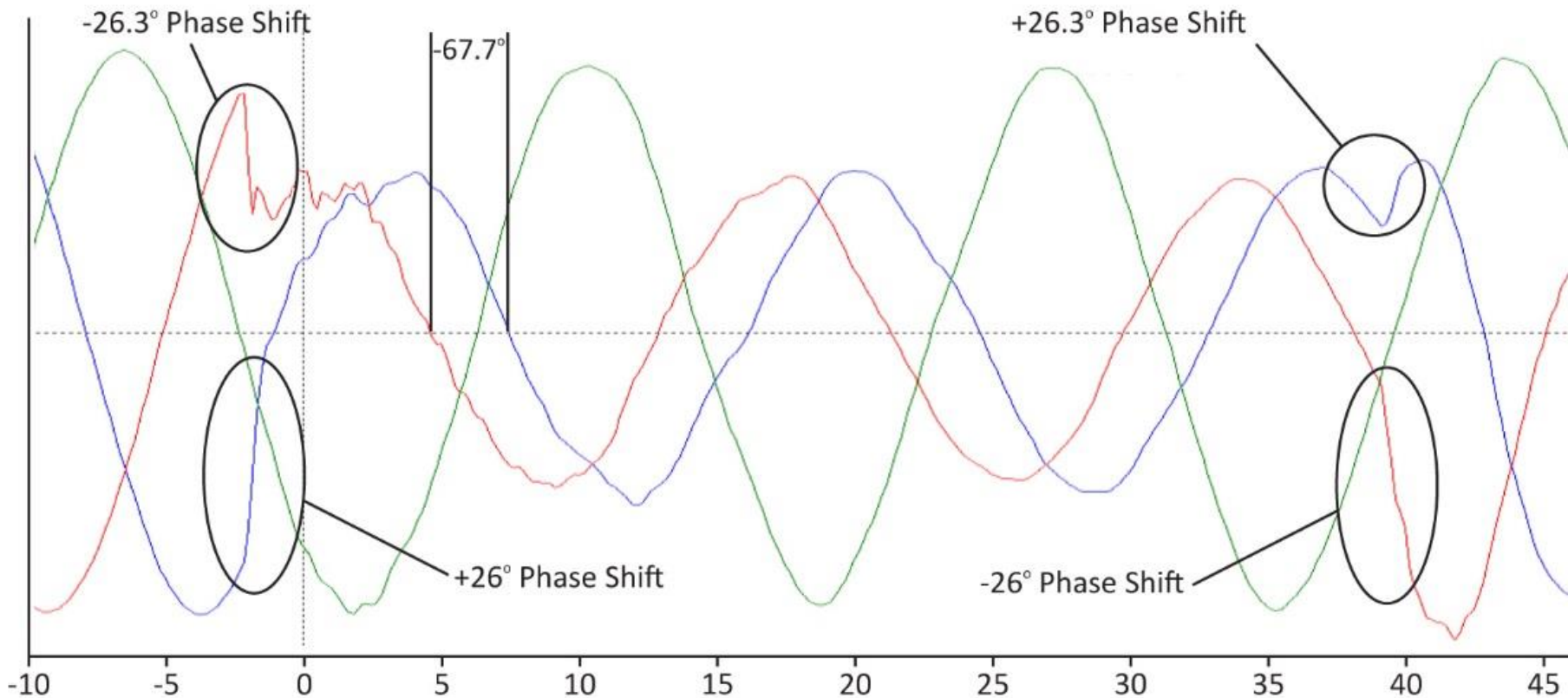
- Largest block of solar PV loss (~700 MW) due to underfrequency tripping
- Inverter sensed a near instantaneous frequency of <57 Hz and tripped instantaneously



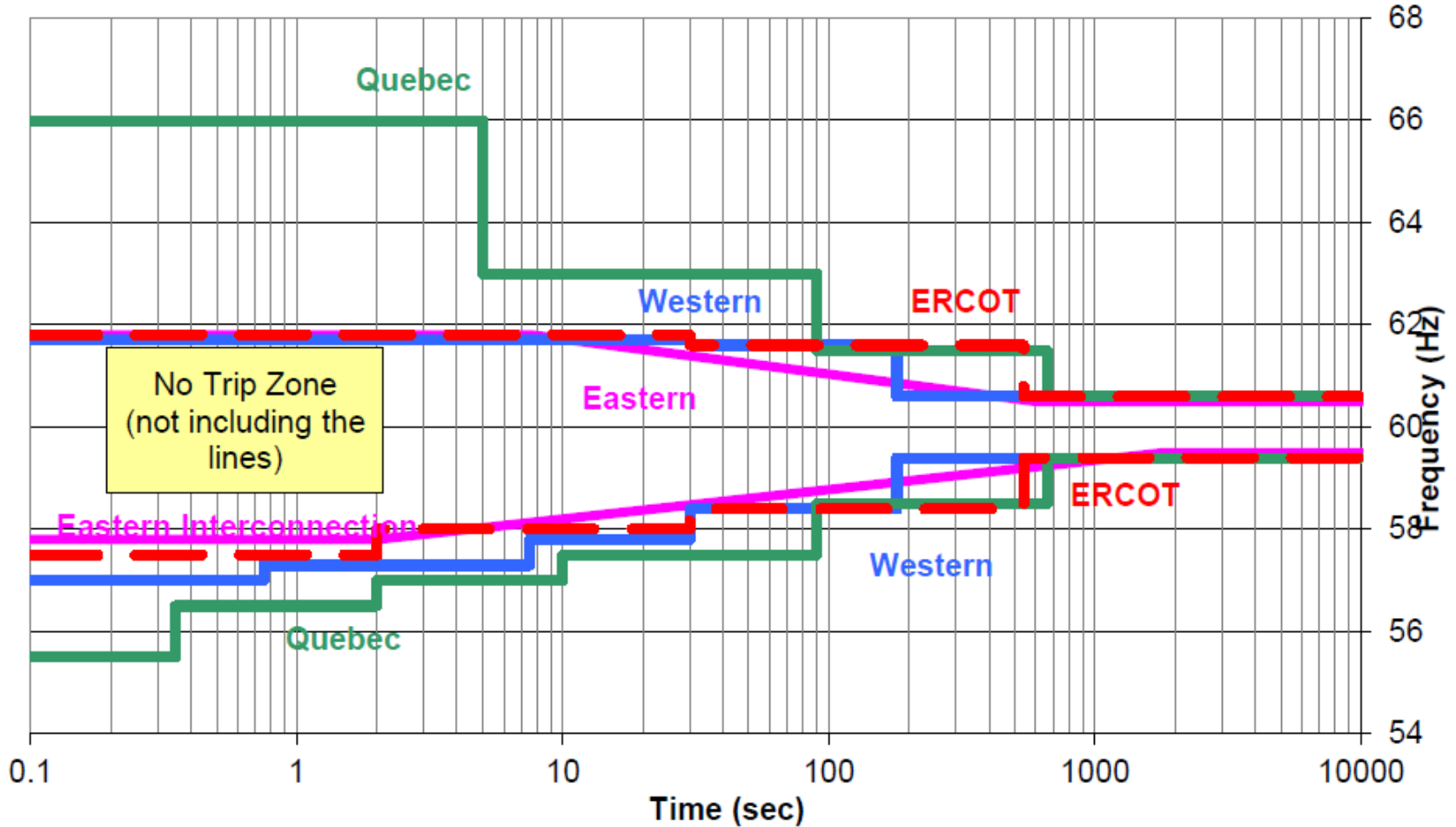
WI\_20160816\_184506

|                   |                     |
|-------------------|---------------------|
| Event ID          | WI_20160816_184506  |
| Event Description | ""                  |
| UTC Time          | 08/16/2016 18:45:06 |
| Local Time        | 08/16/2016 11:45:06 |
| Time Zone         | PDT                 |
| M4 Flag           | Yes                 |
| BAL003 Flag       | Yes                 |
| MW Loss           | 0                   |
| Value A           | 59.979              |
| Value B           | 59.92               |
| Point C           | 59.8669             |
| Time of C         | 4.7                 |
| Point C'          | -                   |
| Time of C'        | -                   |
| A-B [mHz]         | 59                  |
| A-C [mHz]         | 112                 |
| FRM_B [MW/0.1Hz]  | 0                   |
| FRM_C [MW/0.1Hz]  | 0                   |





## OFF NOMINAL FREQUENCY CAPABILITY CURVE



**Curve Data Points:**

**Eastern Interconnection**

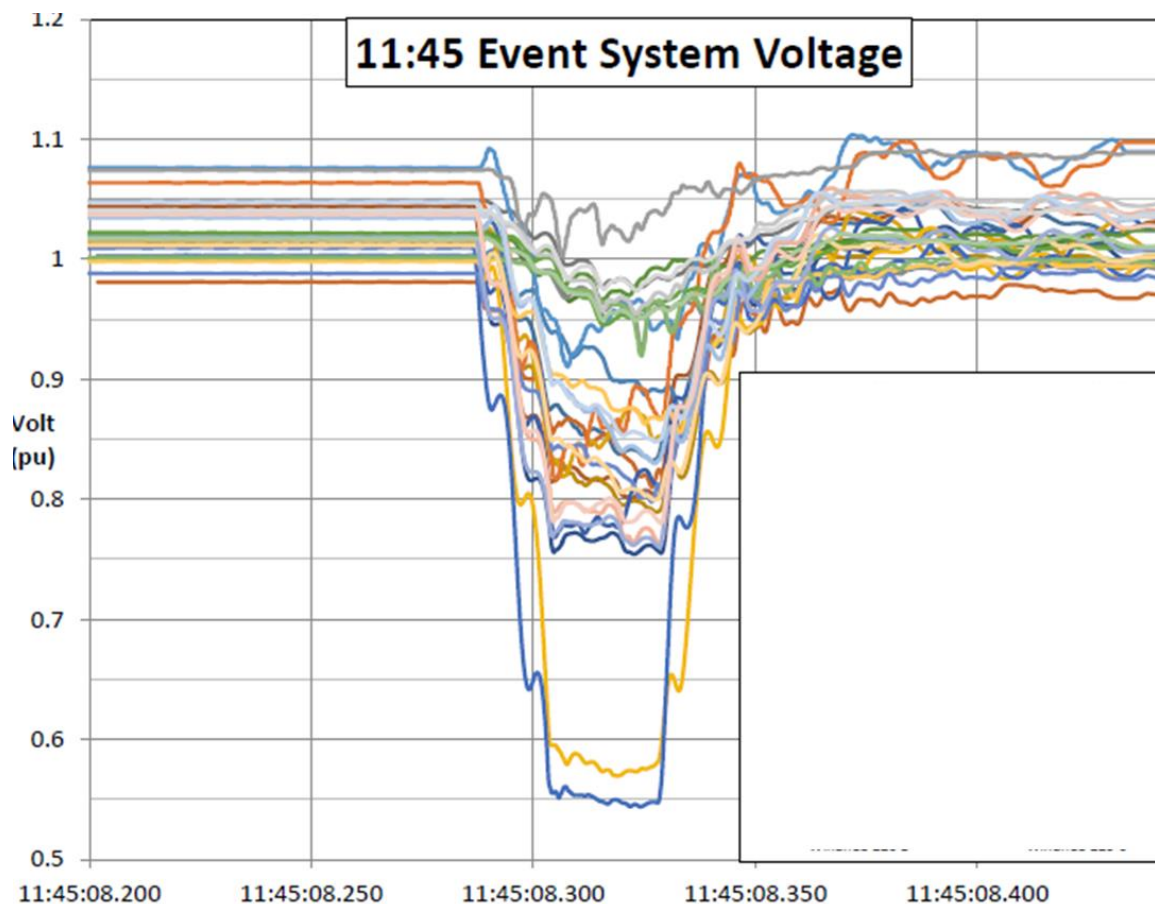
| High Frequency Duration |                           | Low Frequency Duration |                           |
|-------------------------|---------------------------|------------------------|---------------------------|
| Frequency (Hz)          | Time (Sec)                | Frequency (Hz)         | Time (sec)                |
| ≥61.8                   | Instantaneous trip        | ≤57.8                  | Instantaneous trip        |
| ≥60.5                   | $10^{(90.935-1.45713*f)}$ | ≤59.5                  | $10^{(1.7373*f-100.116)}$ |
| <60.5                   | Continuous operation      | > 59.5                 | Continuous operation      |

**Western Interconnection**

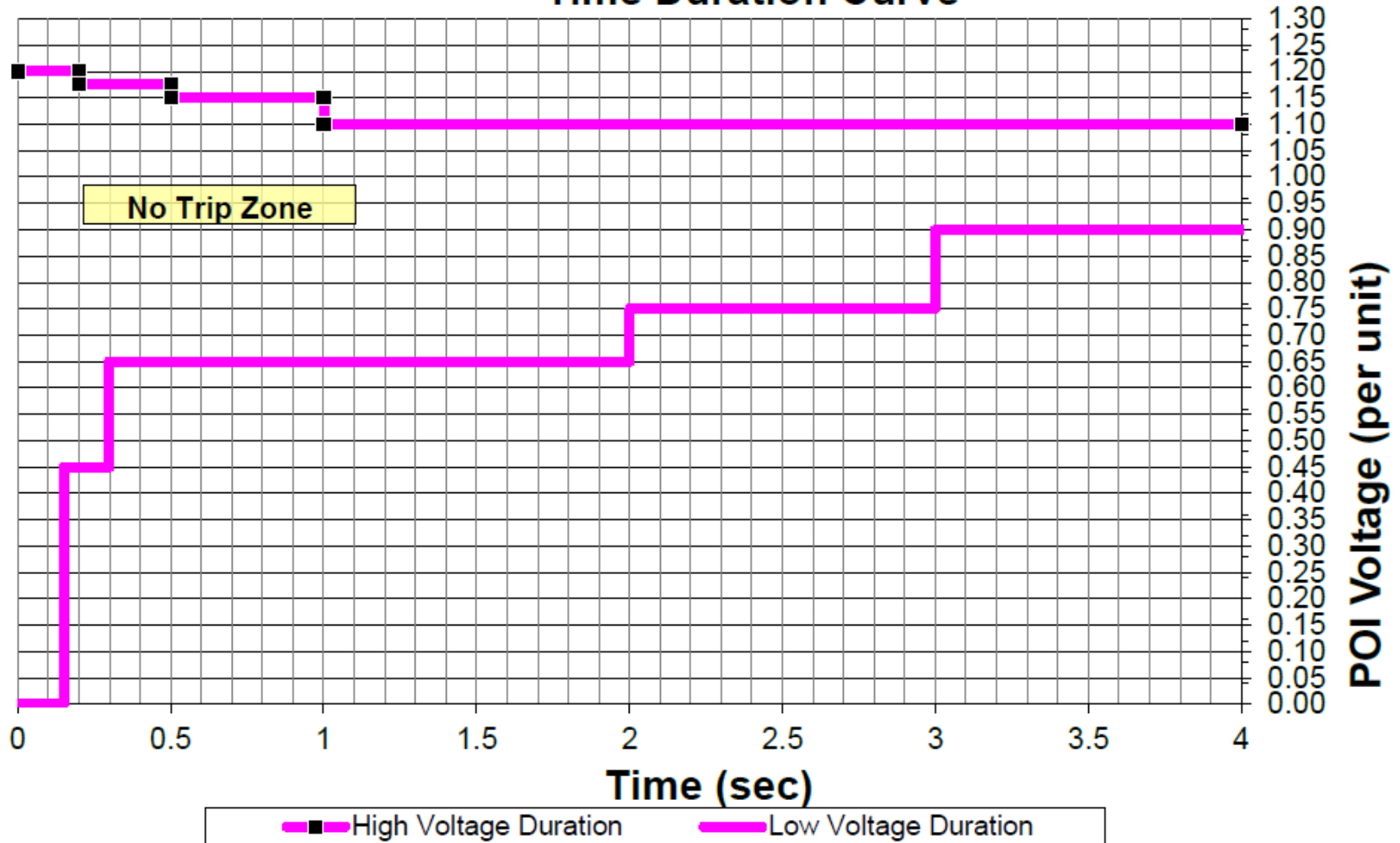
| High Frequency Duration |                      | Low Frequency Duration |                      |
|-------------------------|----------------------|------------------------|----------------------|
| Frequency (Hz)          | Time (Sec)           | Frequency (Hz)         | Time (sec)           |
| ≥61.7                   | Instantaneous trip   | ≤57.0                  | Instantaneous trip   |
| ≥61.6                   | 30                   | ≤57.3                  | 0.75                 |
| ≥60.6                   | 180                  | ≤57.8                  | 7.5                  |
| <60.6                   | Continuous operation | ≤58.4                  | 30                   |
|                         |                      | ≤59.4                  | 180                  |
|                         |                      | >59.4                  | Continuous operation |

- Isolated to one inverter manufacturer
- Manufacturer quickly devised solution following event
- Added time delay to inverter frequency tripping
  - Allows inverter to “ride through” transient/distorted waveform period without tripping.

- 2<sup>nd</sup> largest block of inverter loss (~450 MW) was attributed to low voltage



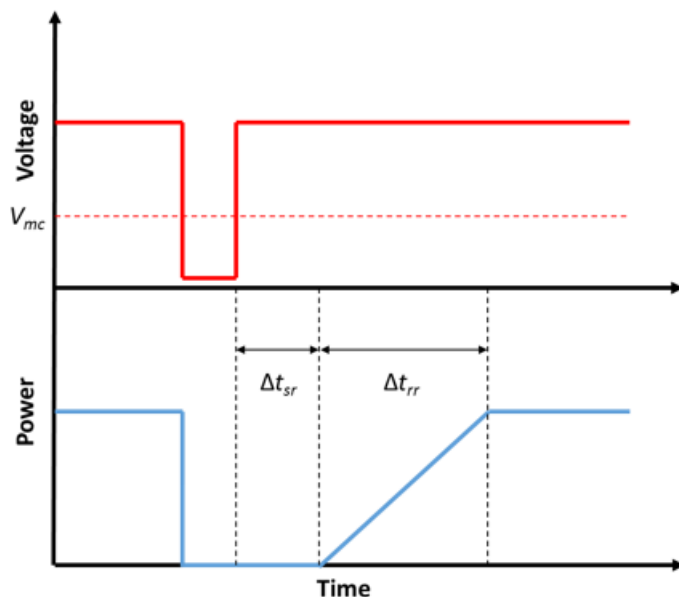
## Voltage Ride-Through Time Duration Curve



- Inverters have three modes of operation
  - Operating (injecting active current into the system)
  - Momentary Cessation (momentarily cease to inject current during voltages outside continuous operating range - .9 to 1.0 per unit)
  - Trip (cease to inject current, disconnect from grid, wait ~ five minutes and return to service if grid voltage and frequency are within bounds)

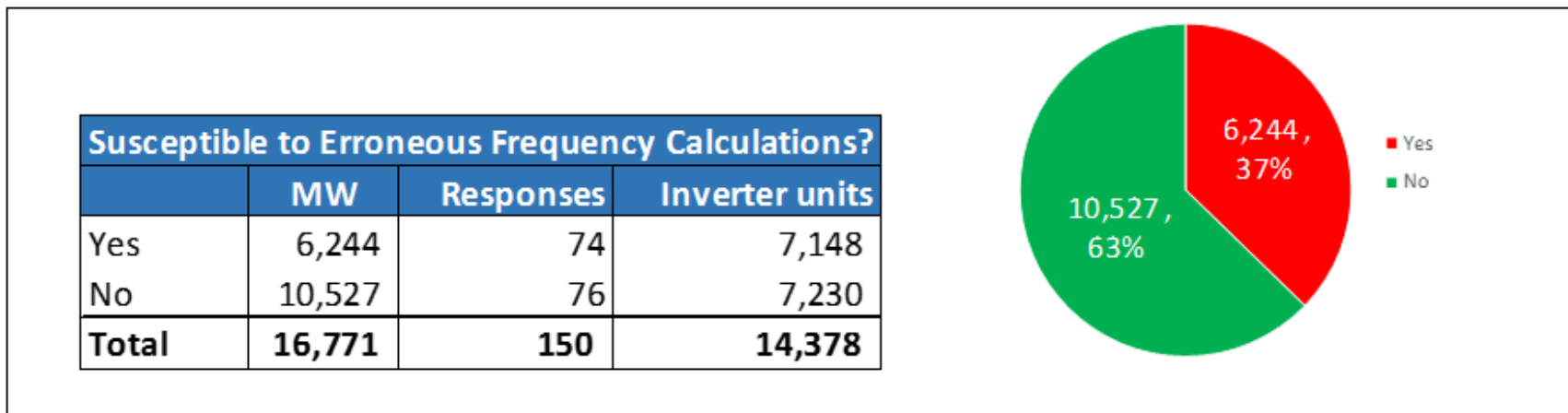


- The inverters did not “Trip”, they went into Momentary Cessation
- Majority of installed inverters set to momentarily cease current injection for voltages of  $V < .9$  p.u. or  $V > 1.1$  p.u.
- In inverter language, Momentary Cessation does not equal trip

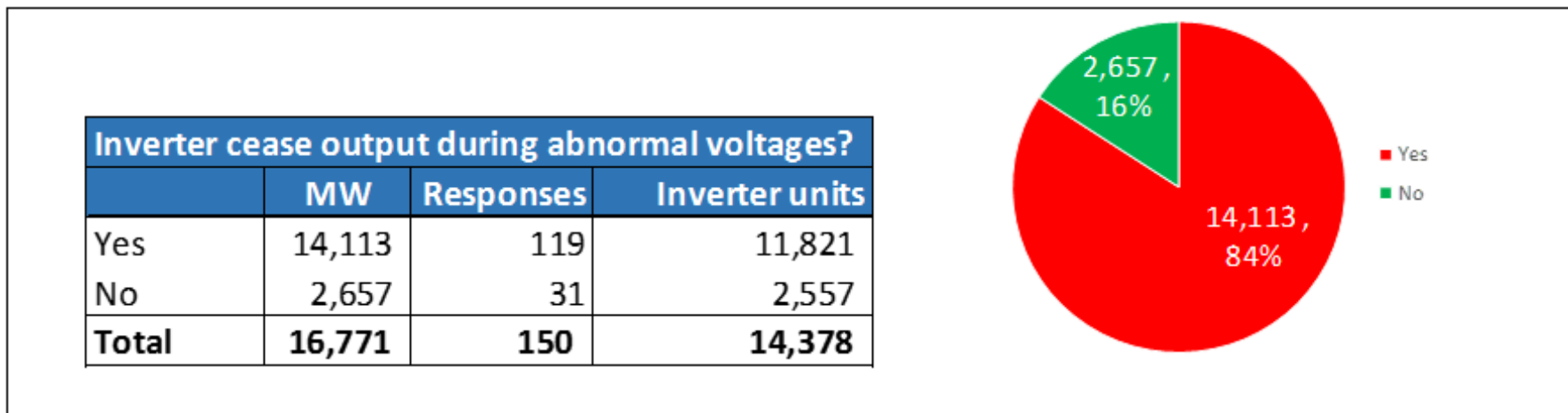


- Frequency tripping
  - Manufacturer is adding tripping delay
- Simulations to identify momentary cessation risk
  - ~7200 MW potential
  - Specify maximum delay and ramp rate for Restore Output

- NERC Alert/Recommendation to Industry was issued 6/20/2017
  - Work with inverter manufacturer to ensure no erroneous frequency tripping
  - If momentary cessation is used, restore output in no more than 5 seconds



**Figure 2: MW susceptible to Erroneous Frequency Calculations**

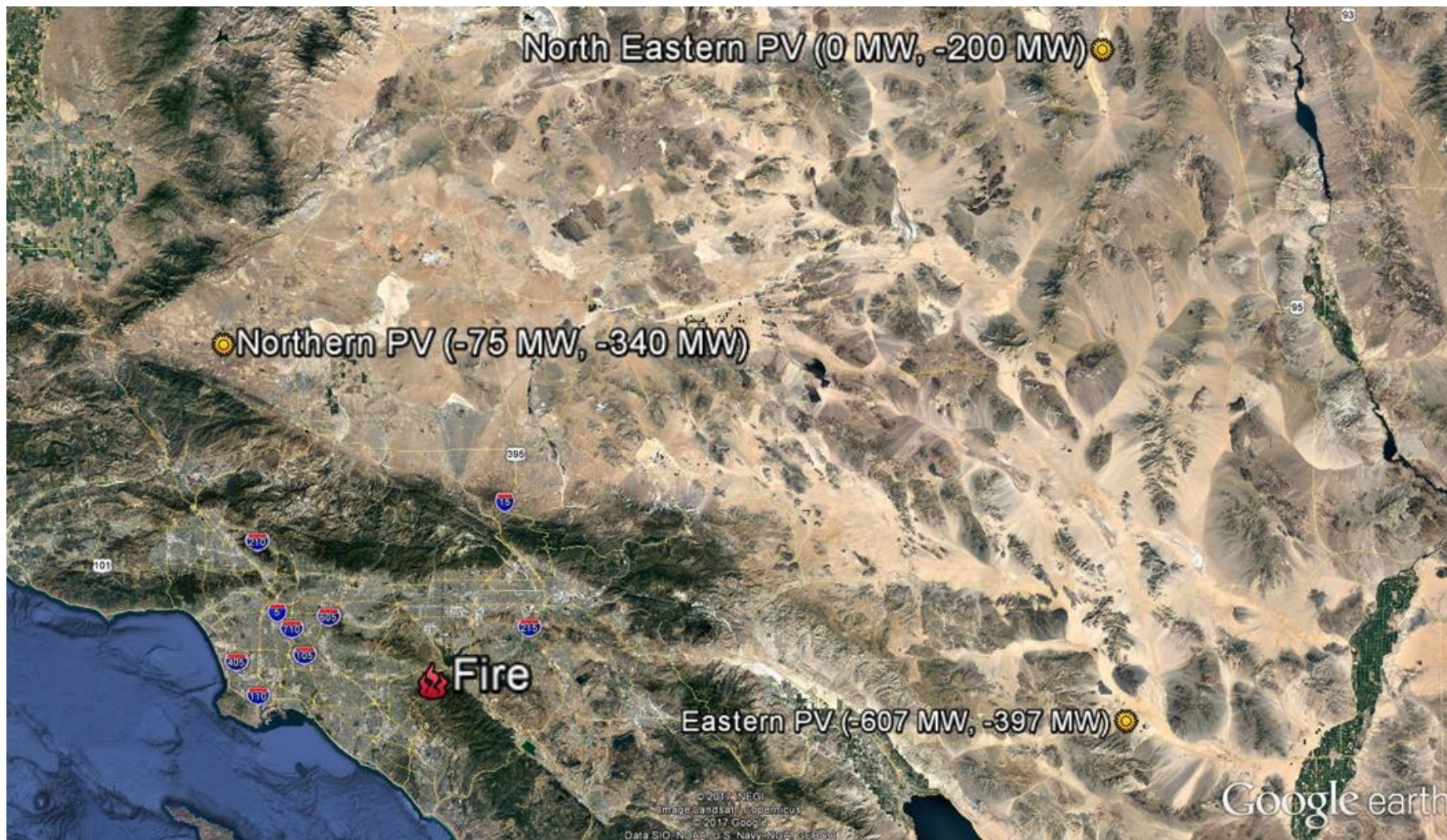


**Figure 4: MW cease output during abnormal voltages**

- Further study needed for risk associated with momentary cessation (IRPTF)
- Clarify that outside the PRC-024 frequency and voltage ride-through curves are may trip, not must trip
- Review PRC-024 to determine if any changes are needed

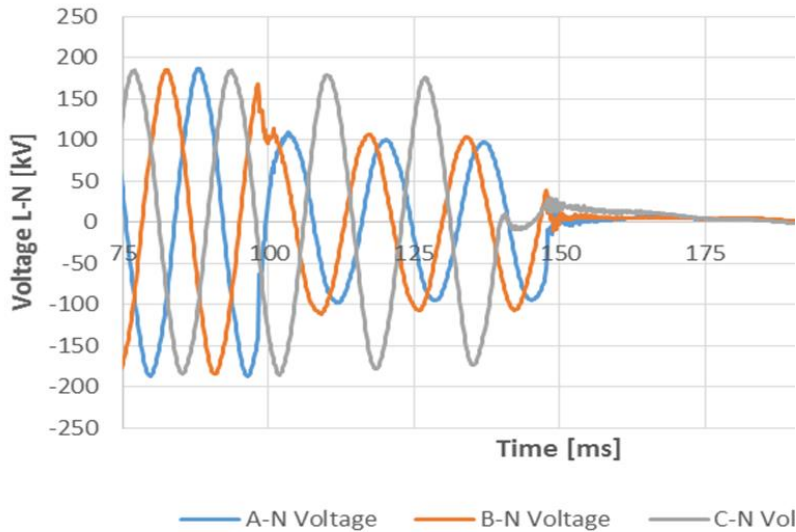
**October 9, 2017**  
**Canyon 2 Fire Disturbance**

*Key Findings and Recommendations*

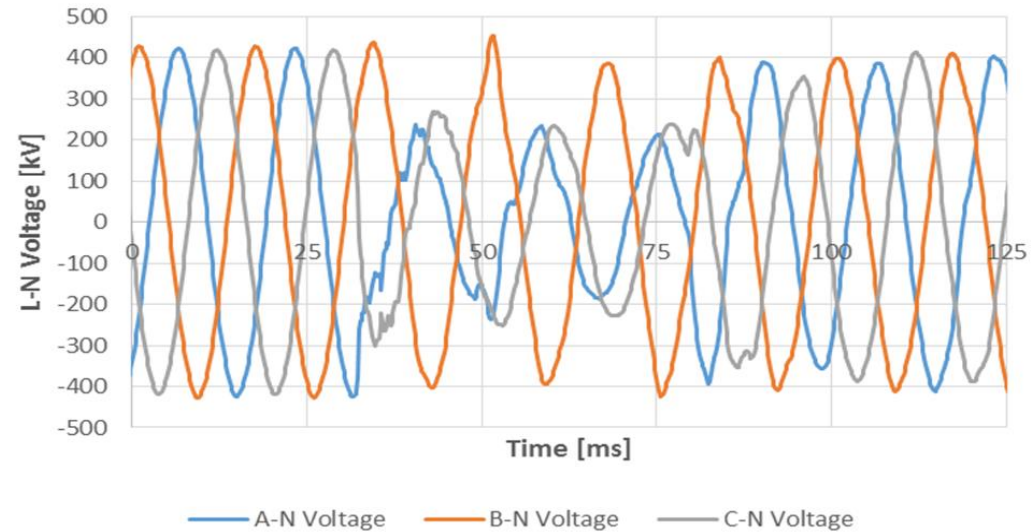




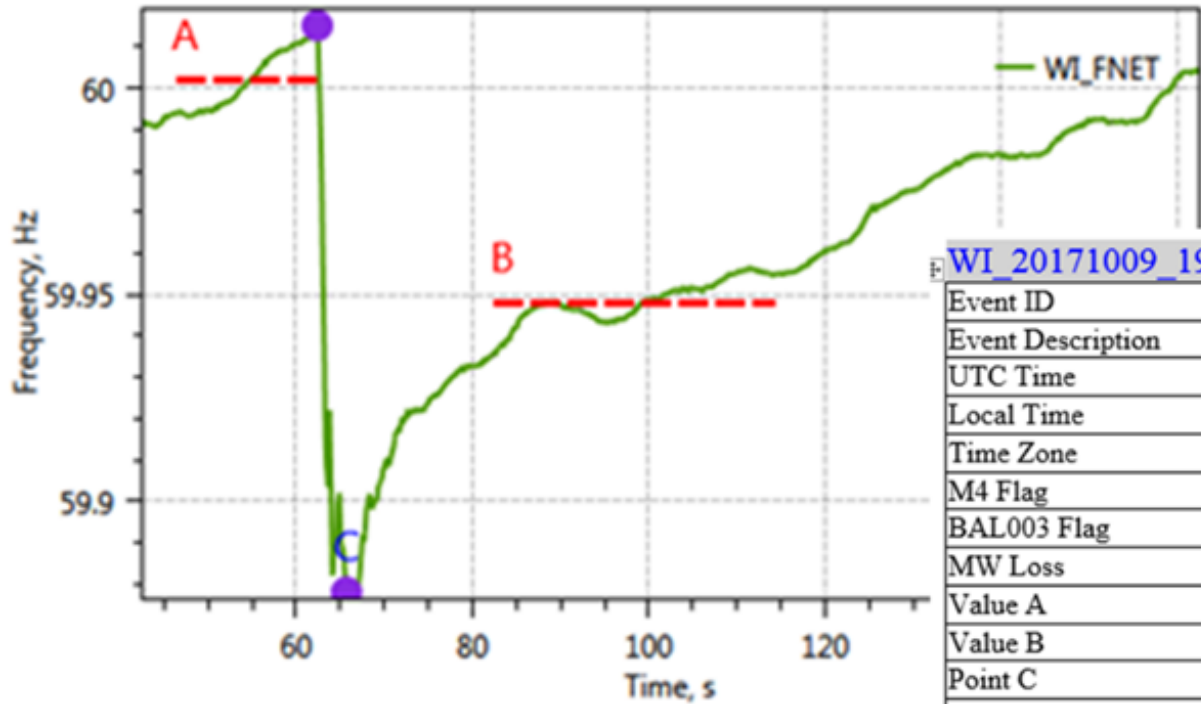
*Smoke-induced L-L fault events caused by Canyon 2 Fire...  
Both fault cleared normally...*



**Fault Event 1:**  
**220 kV**  
**L-L Fault**  
**< 3 cycle clearing**

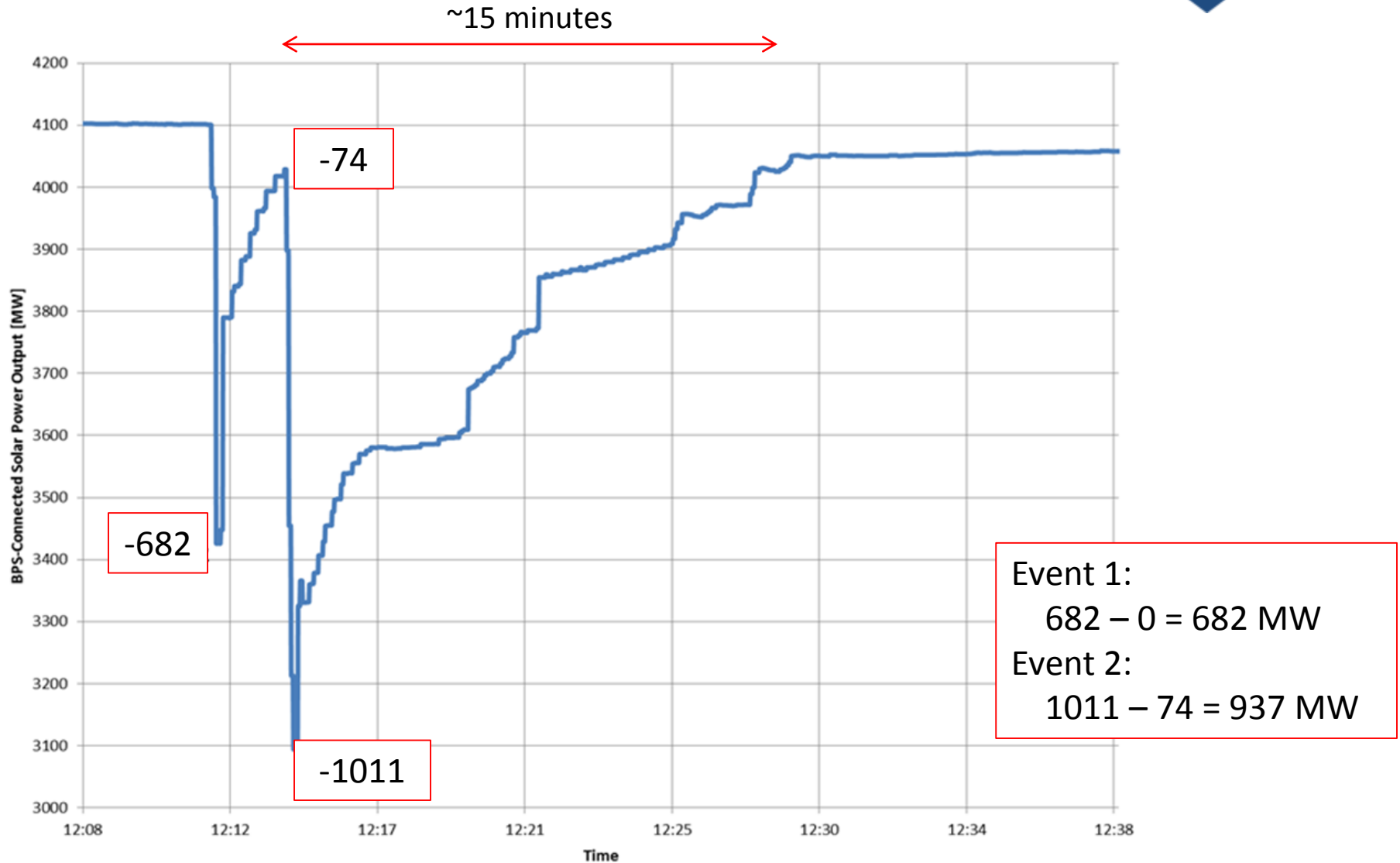


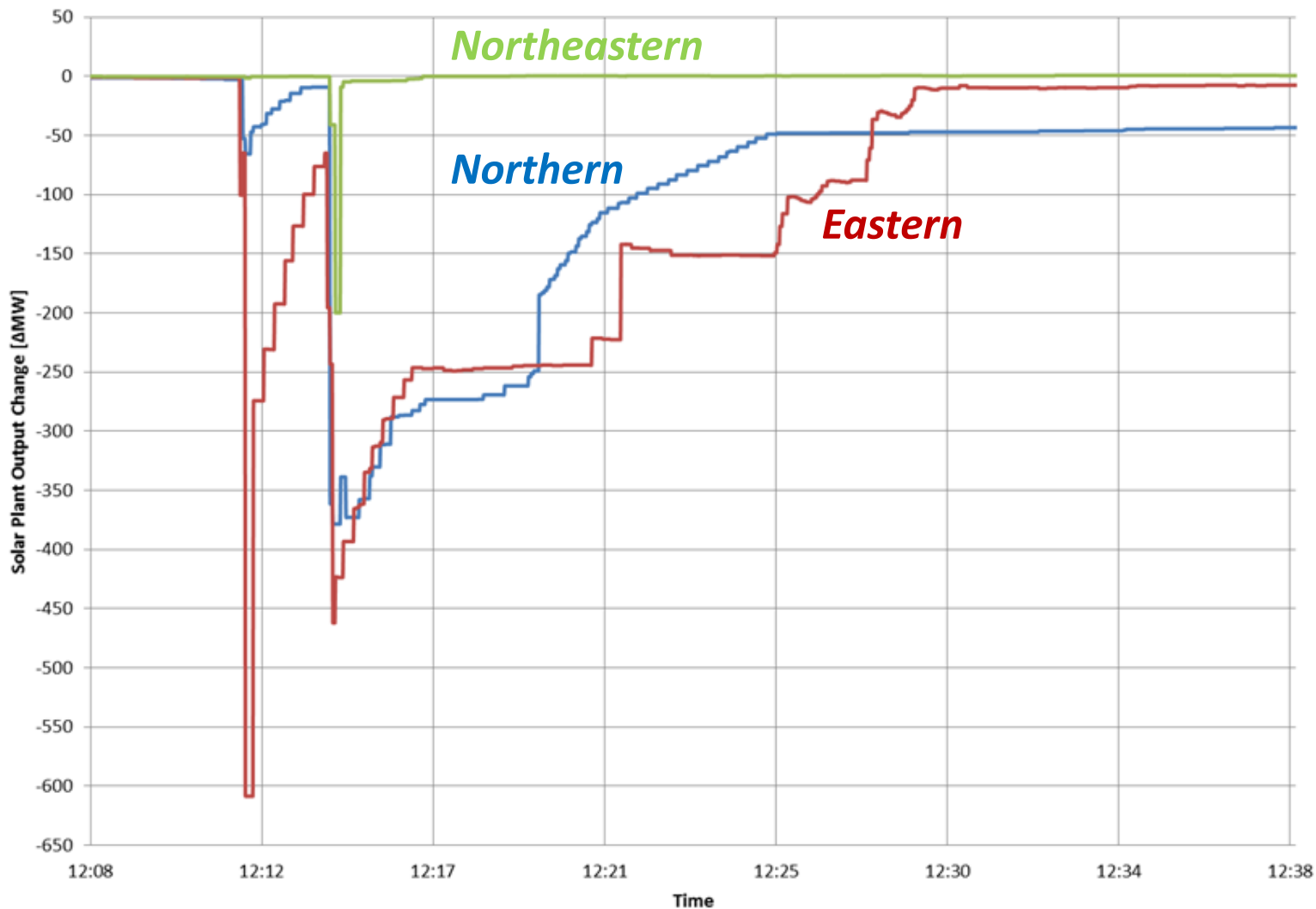
**Fault Event 2:**  
**500 kV**  
**L-L Fault**  
**< 3 cycle clearing**

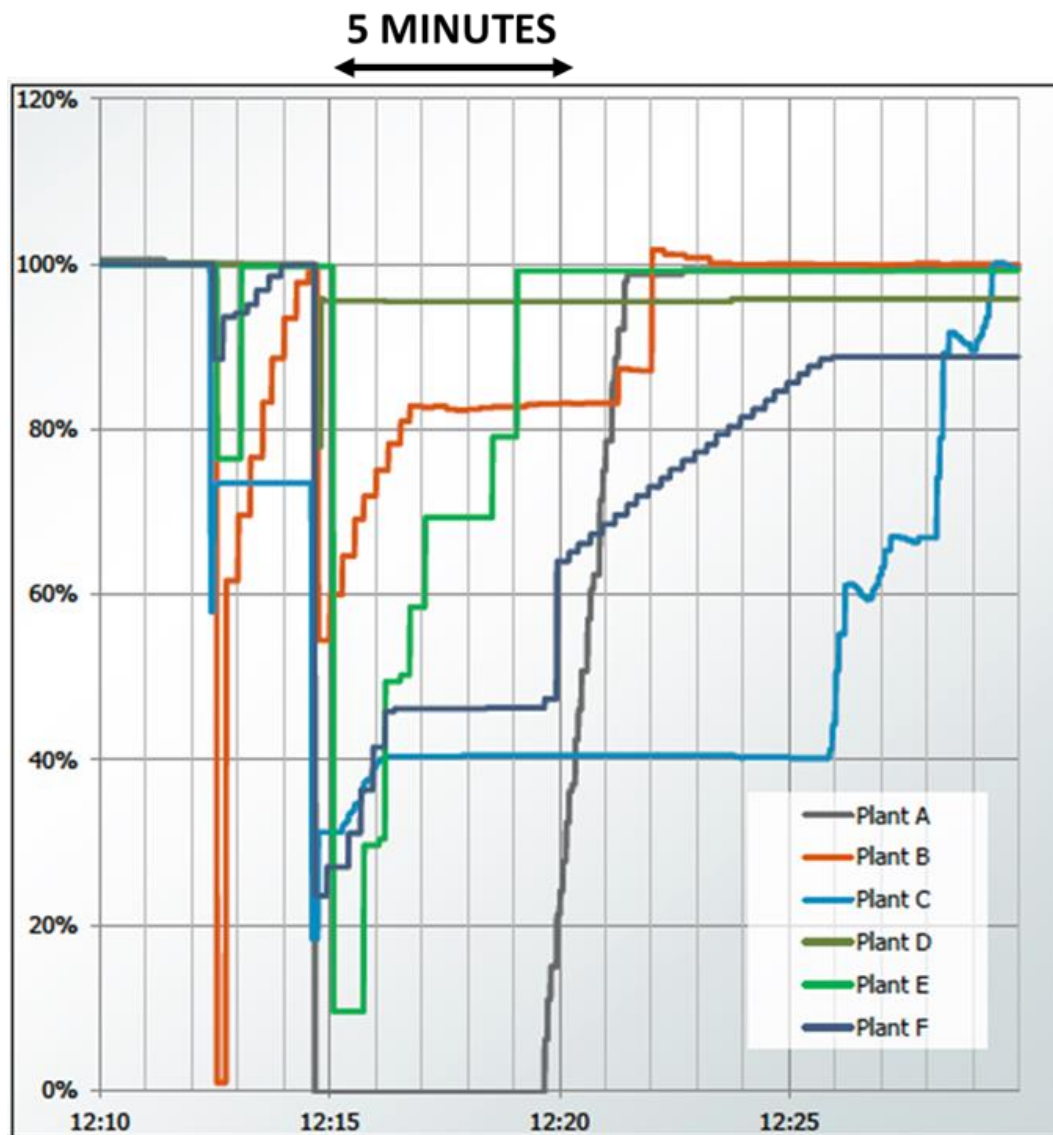


WI\_20171009\_191428

|                   |                               |
|-------------------|-------------------------------|
| Event ID          | WI_20171009_191428            |
| Event Description | "Solar Generation 900MW loss" |
| UTC Time          | 10/09/2017 19:14:28           |
| Local Time        | 10/09/2017 12:14:28           |
| Time Zone         | PDT                           |
| M4 Flag           | Yes                           |
| BAL003 Flag       | Yes                           |
| MW Loss           | 900                           |
| Value A           | 60.002                        |
| Value B           | 59.948                        |
| Point C           | 59.878                        |
| Time of C         | 3.3                           |
| Point C'          | -                             |
| Time of C'        | -                             |
| A-B [mHz]         | 54                            |
| A-C [mHz]         | 124                           |
| FRM_B [MW/0.1Hz]  | 1667                          |
| FRM_C [MW/0.1Hz]  | 726                           |







1. No erroneous frequency tripping
2. Continued use of momentary cessation
3. Ramp rate interactions with return from momentary cessation
4. Interpretation of PRC-024-2 voltage ride-through curve
5. Instantaneous voltage tripping and measurement filtering
6. Phase lock loop synchronization issues
7. DC reverse current tripping
8. Transient interactions and ride-through considerations

## *No erroneous frequency tripping*

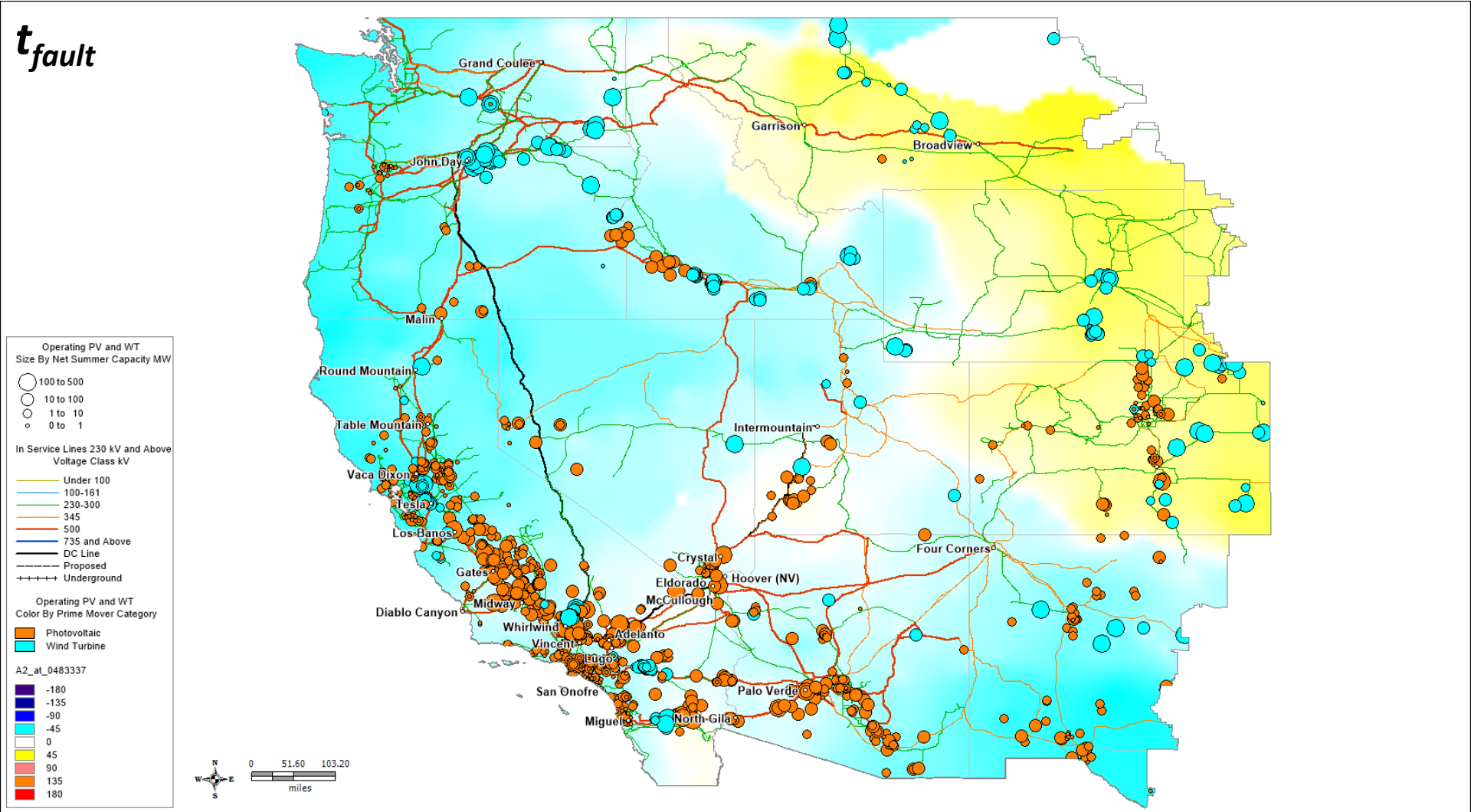
- Alert recommended GOPs and GOs ensure inverter controls do not erroneously trip on instantaneous frequency measurements
- By October 9, 2017 event, 97% of inverter manufacturer's BPS-connected fleet had been updated
- Mitigating actions by inverter manufacturer and GOs appear to have worked

### *Continued use of momentary cessation*

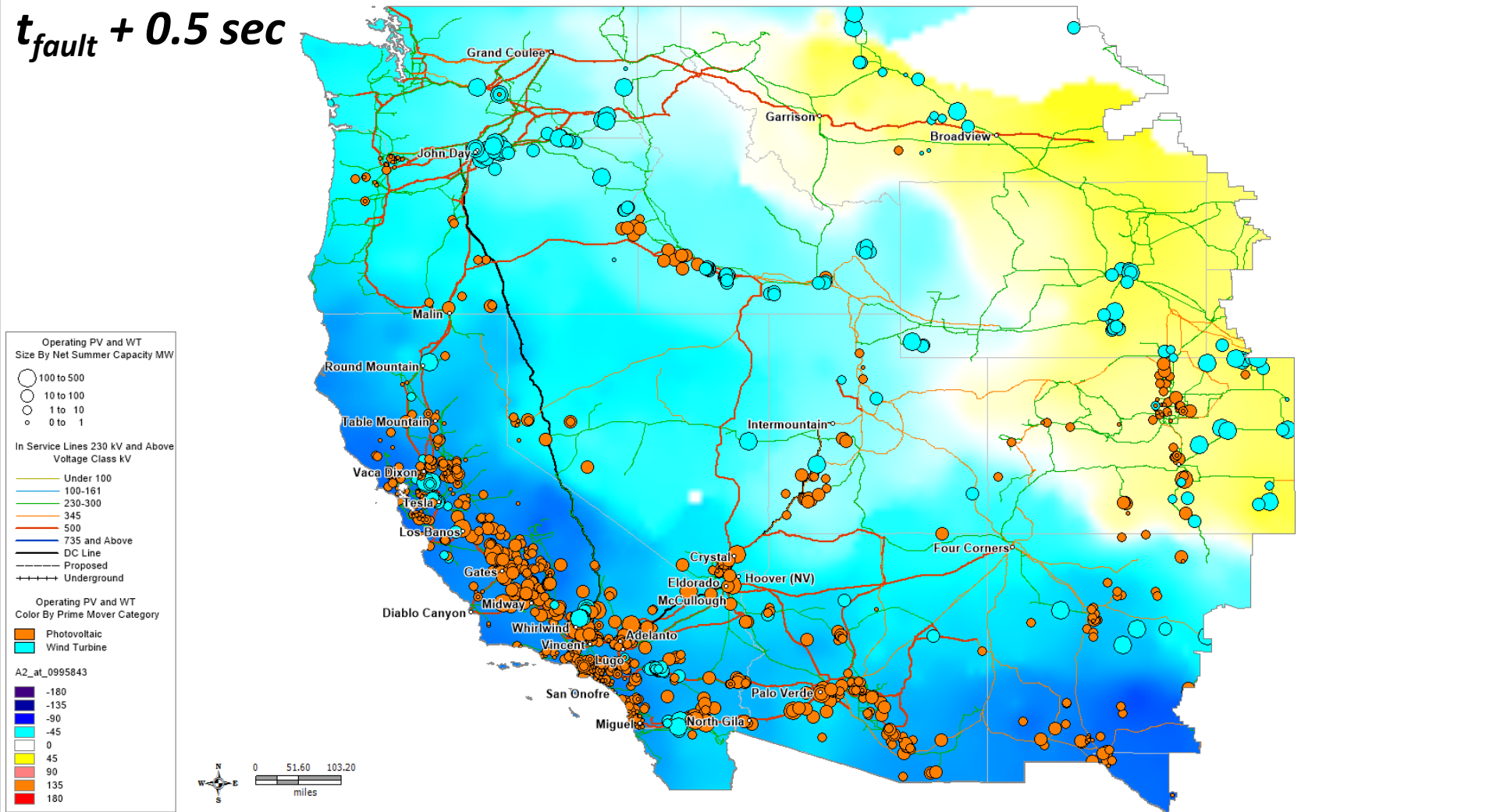
- Majority of existing inverters use momentary cessation
- Most use a low voltage threshold of  $\sim 0.9$  pu
- Recovery of current following momentary cessation varies, relatively slow for grid dynamics
- Blue Cut Fire recommendation – interim solution
- NERC IRPTF studies – new recommendation
  - Stability studies show potential BPS wide-area stability issues



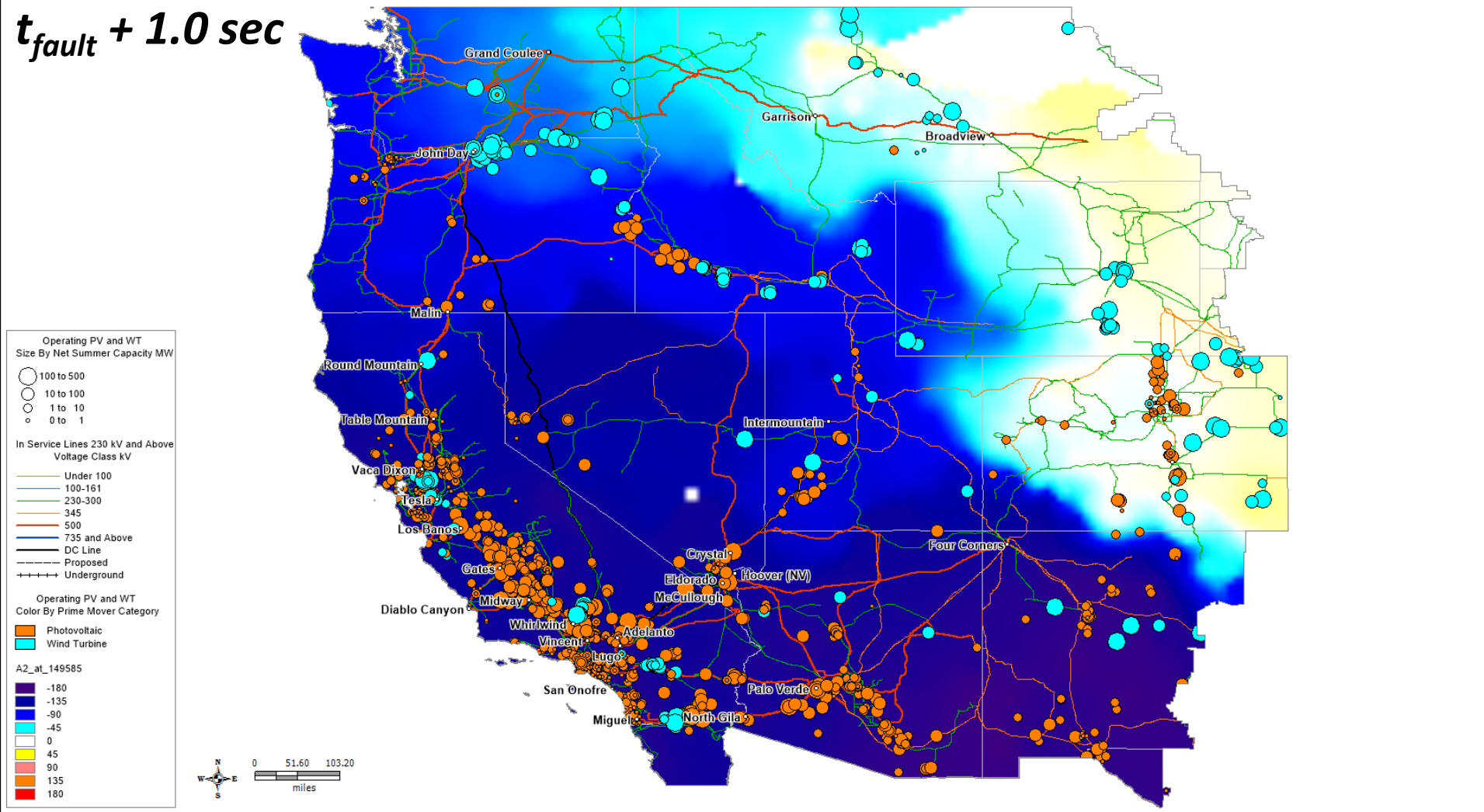
$t_{fault}$



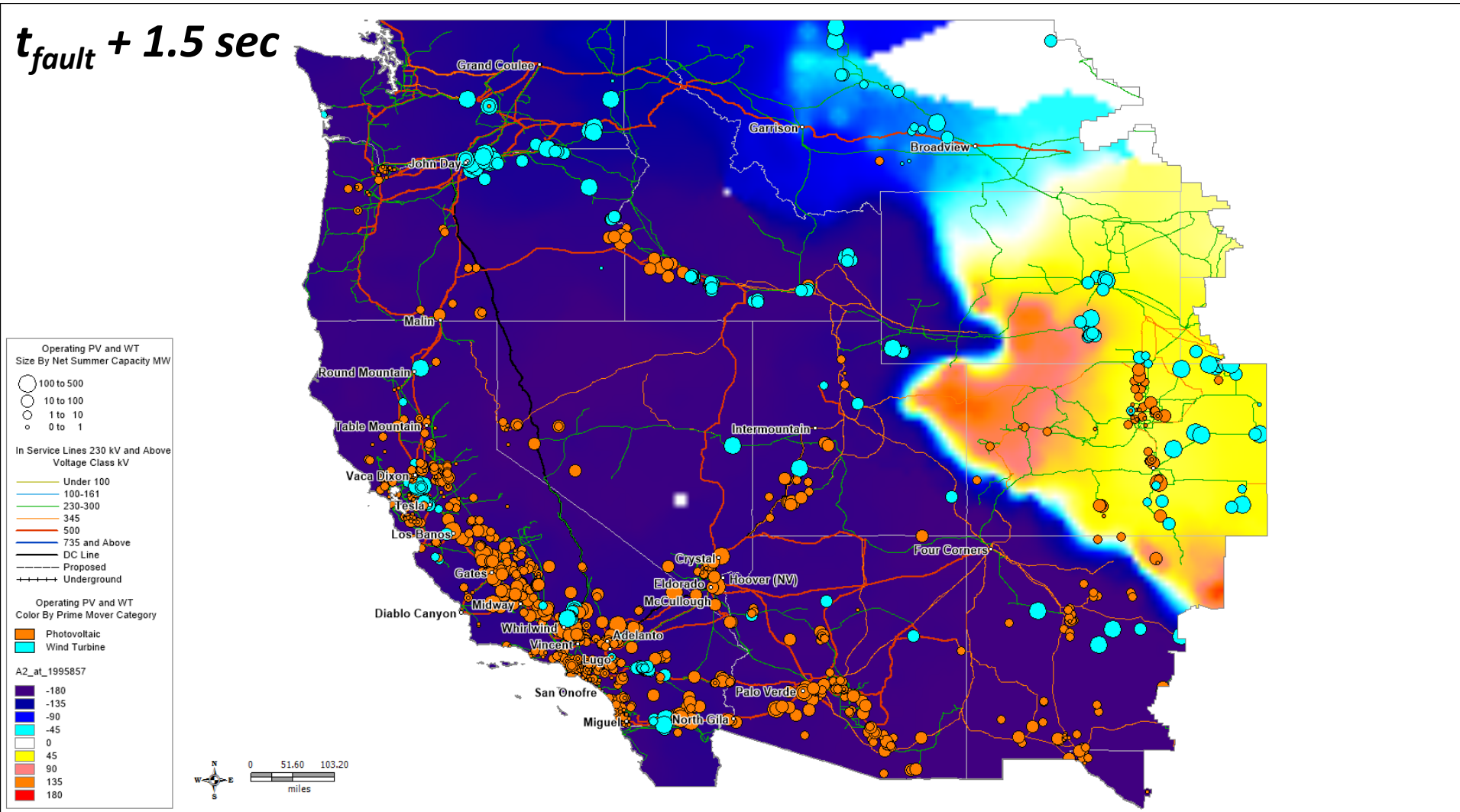
$t_{fault} + 0.5 \text{ sec}$



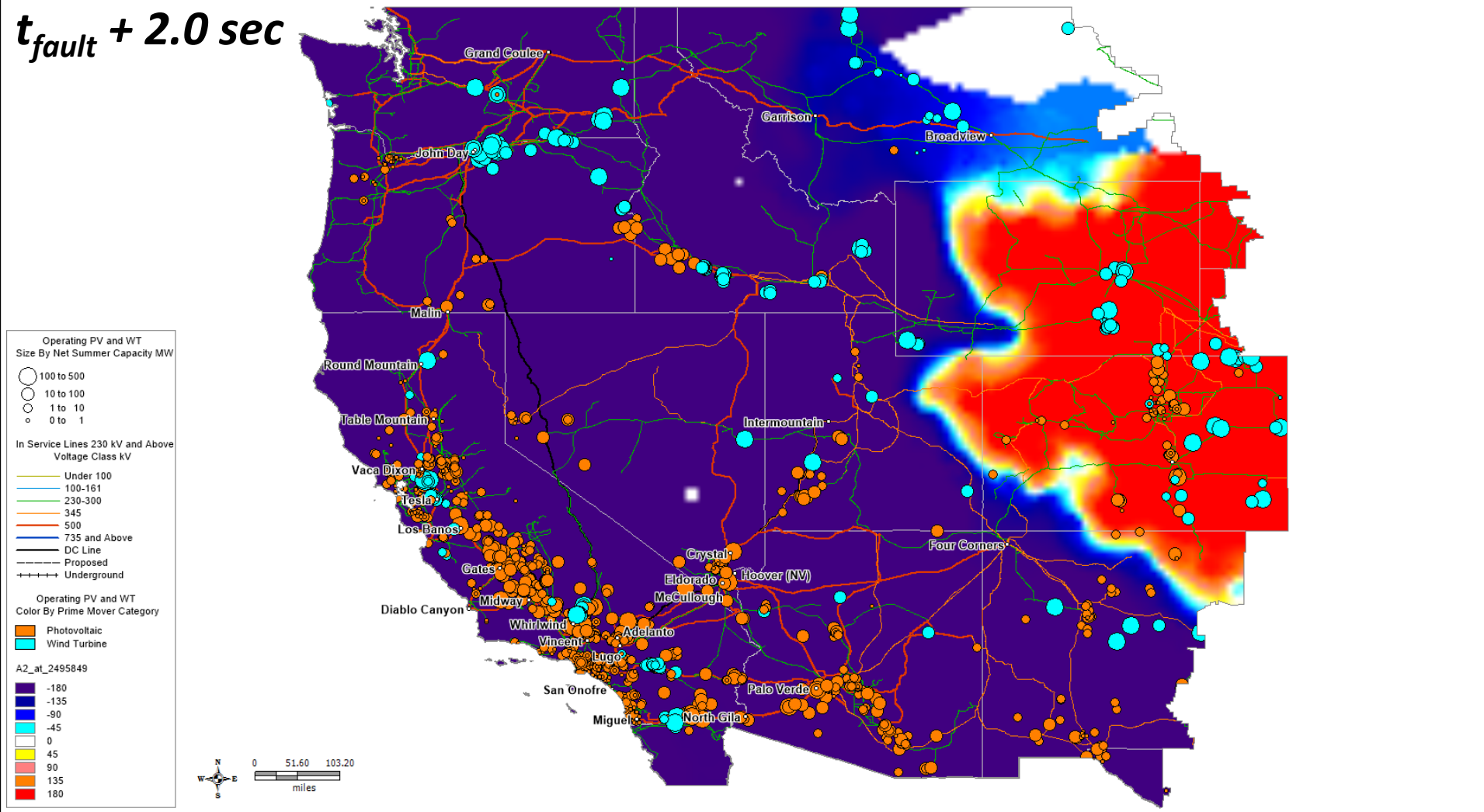
$t_{fault} + 1.0 \text{ sec}$



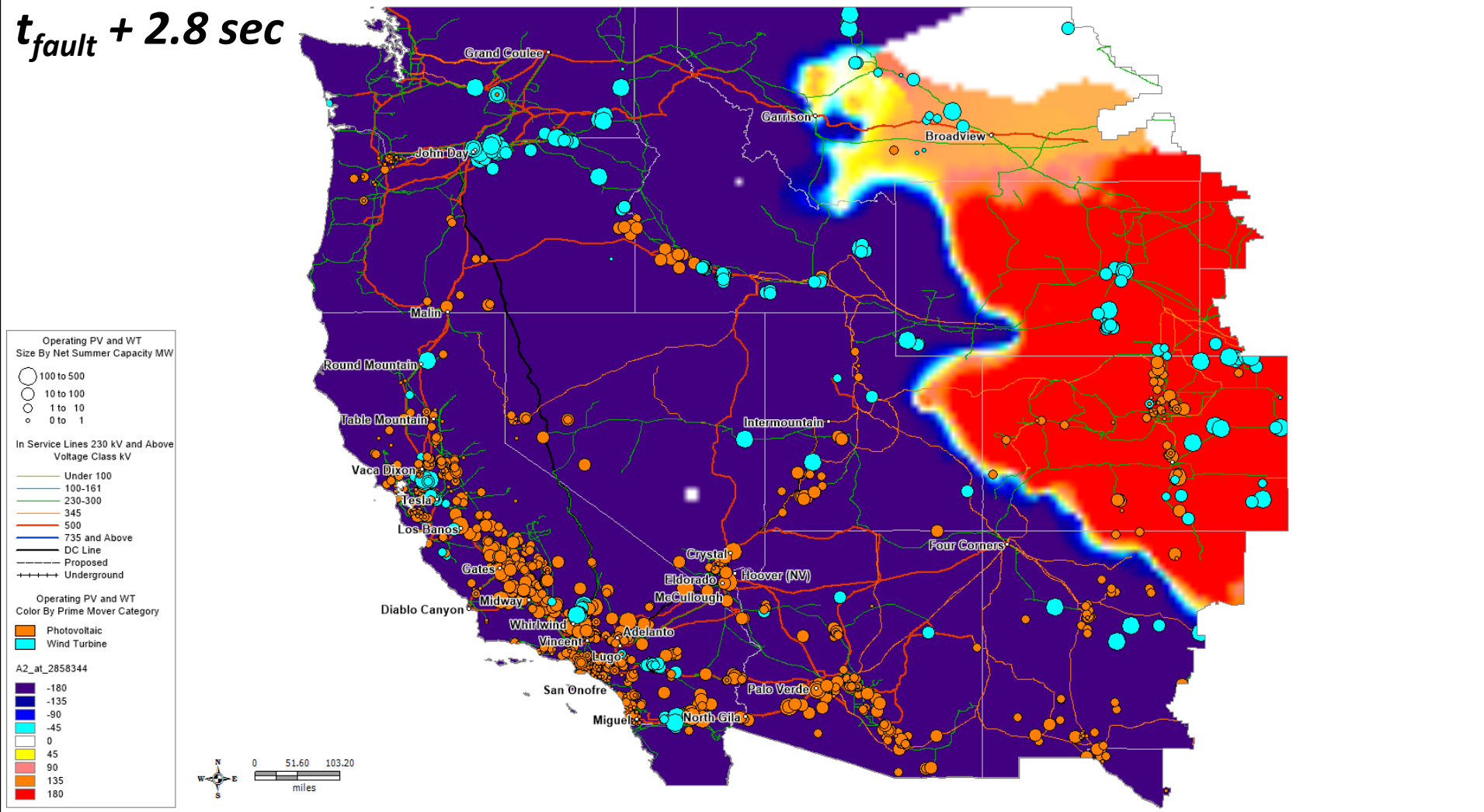
$t_{fault} + 1.5 \text{ sec}$



$t_{fault} + 2.0 \text{ sec}$

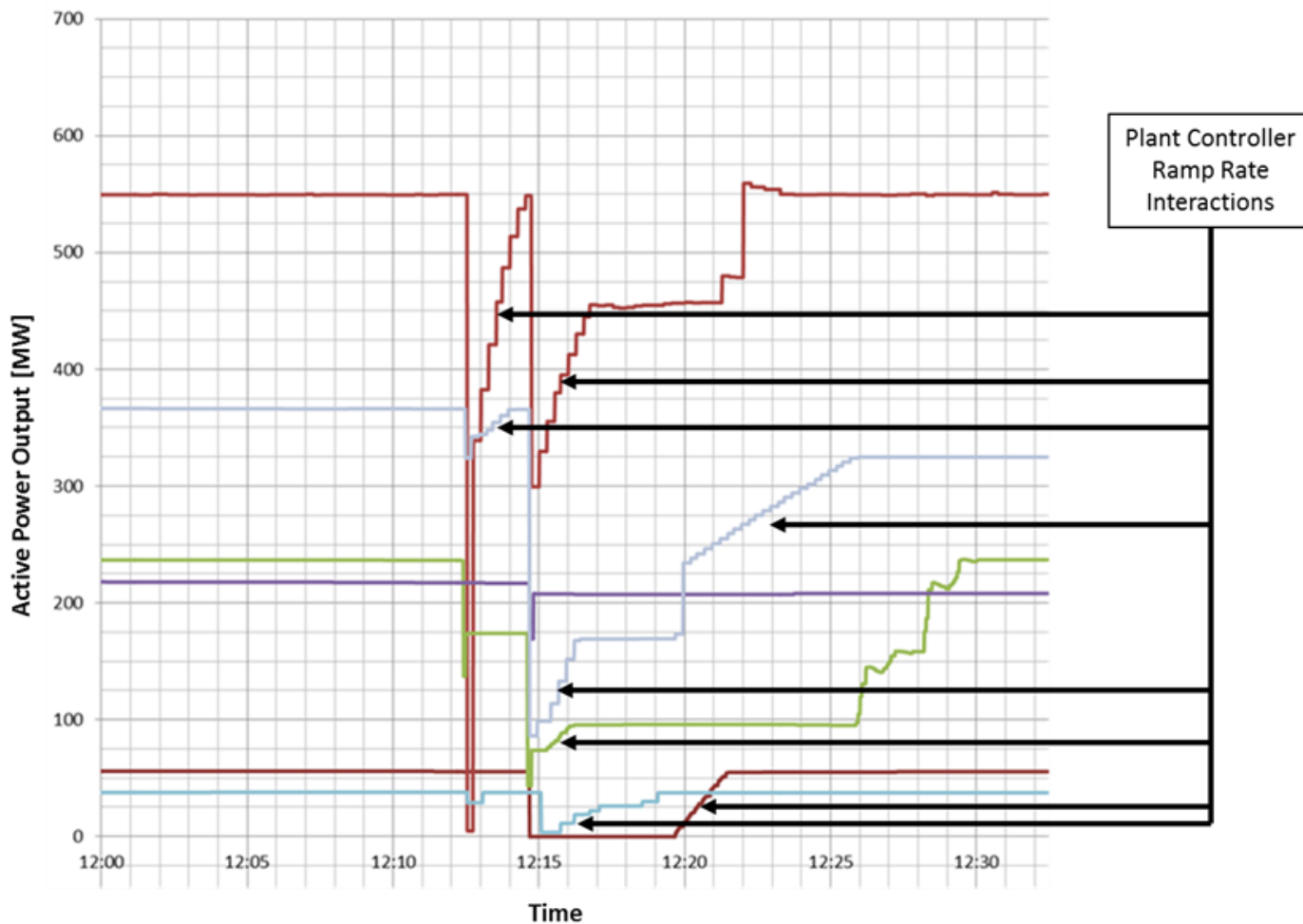


$t_{fault} + 2.8 \text{ sec}$



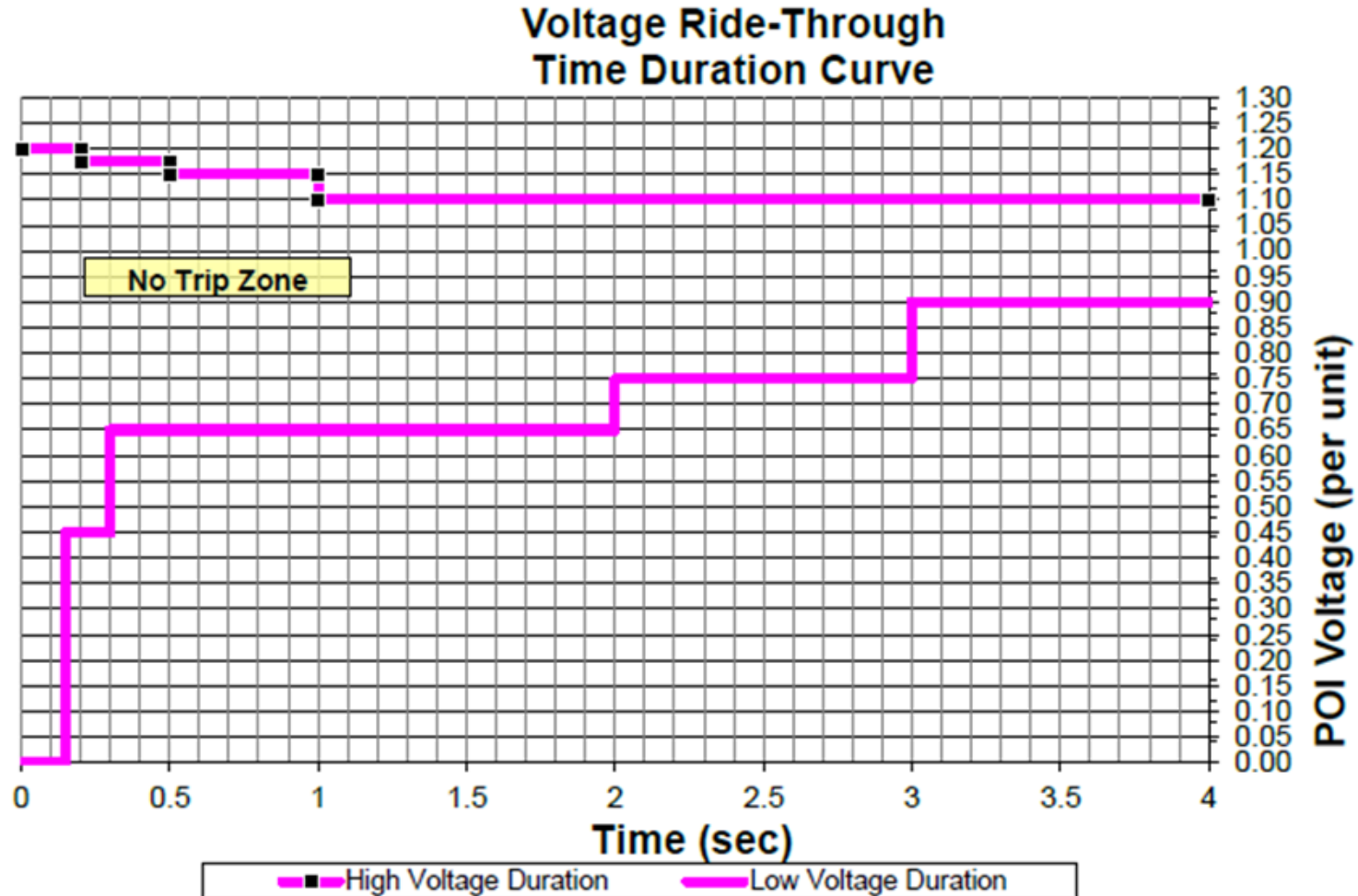
- Generator Owners should coordinate with their inverter manufacturer(s) to **eliminate momentary cessation (MC) to the greatest extent possible.**
- For inverters where MC cannot be eliminated (e.g., use another form of ride-through mode), MC settings should be changed by:
  - Reducing the MC low voltage threshold to the lowest value possible.
  - Reducing the recovery delay to the smallest value possible (e.g., on the order of 1-3 electrical cycles).
  - Increasing the active power ramp rate to at least 100% per second (e.g., return to pre-disturbance active current injection within 1 second).
  - Setting reactive current priority upon recovery (if applicable) should eliminate the use of MC on all inverters that are capable of continuous current injection during abnormal voltages.

## *Ramp rate interactions with return from momentary cessation*

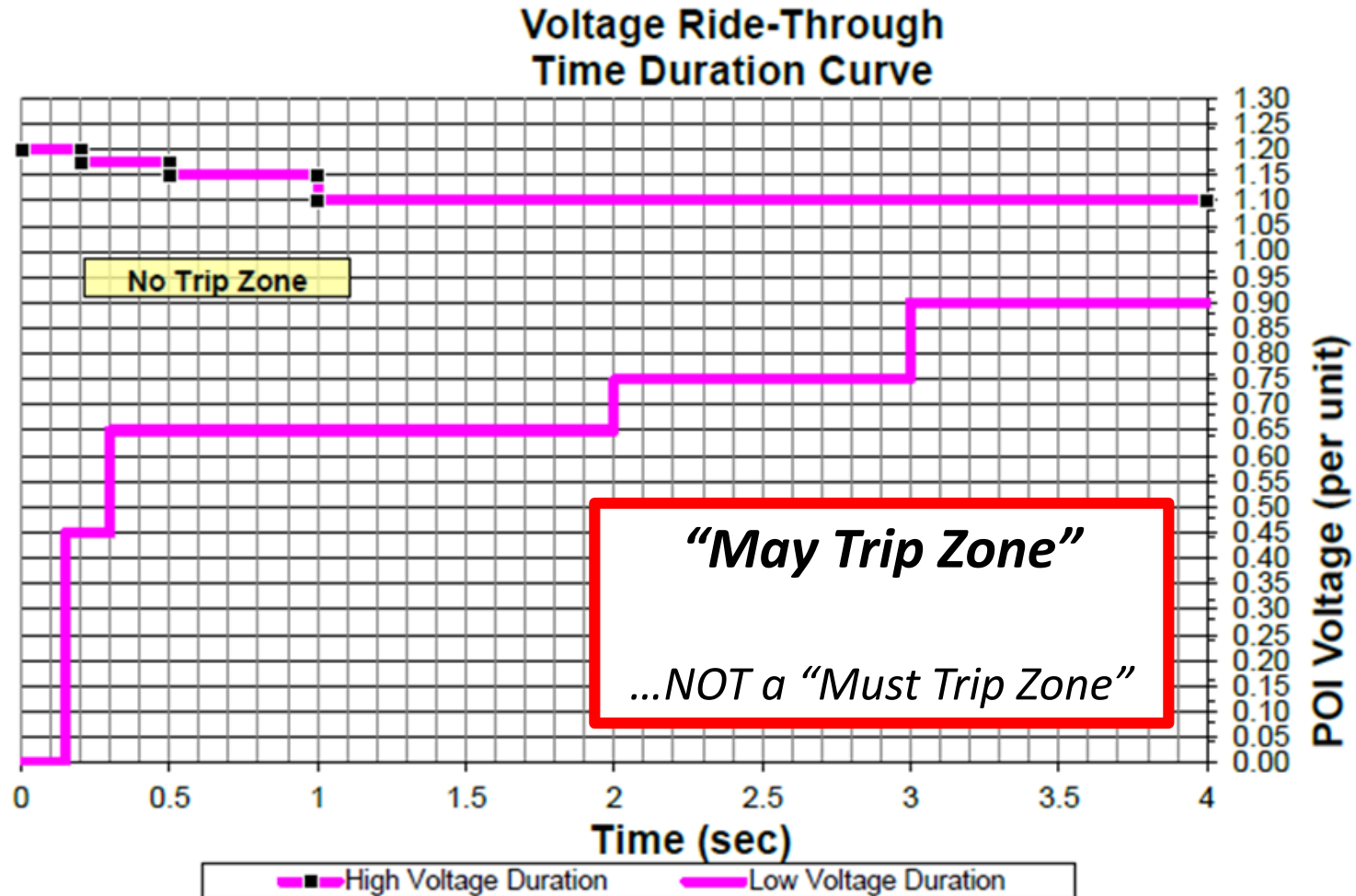




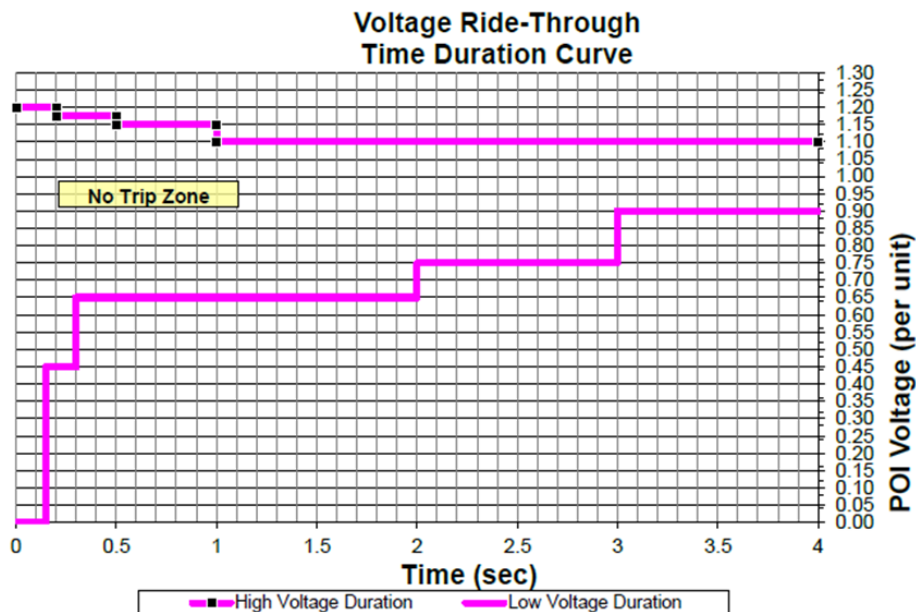
*Interpretation of PRC-024-2 voltage ride-through curve*



*Interpretation of PRC-024-2 voltage ride-through curve*



*Interpretation of PRC-024-2 voltage ride-through curve*



**This curve is a minimum requirement.**

This curves should NOT be a design criteria.

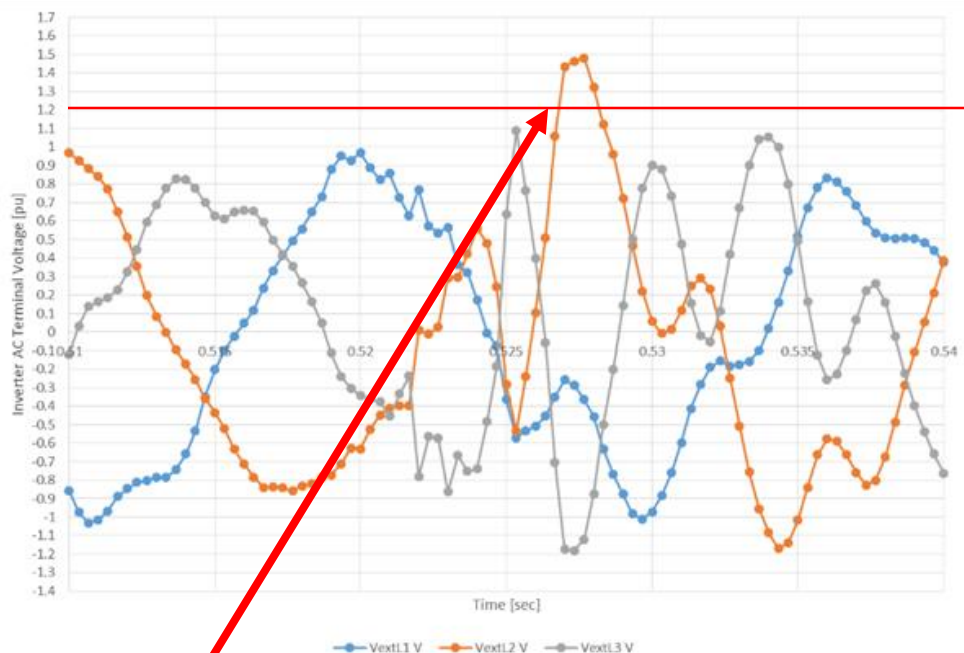
Protection should be set based on equipment limitations.

Equipment should be designed as robust as possible.

*Interpretation of PRC-024-2 voltage ride-through curve*

- **Requirement R2:** Each Generator Owner that has generator voltage protective relaying<sup>1</sup> activated to trip its applicable generating unit(s) shall set its protective relaying such that the generator voltage protective relaying does not trip the applicable generating unit(s) as a result of a voltage excursion (at the point of interconnection<sup>3</sup>) caused by an event on the transmission system external to the generating plant that remains within the “no trip zone” of PRC-024 Attachment 2.
- **Footnote 3:** For the purposes of this standard, point of interconnection means the transmission (high voltage) side of the generator step-up or collector transformer.

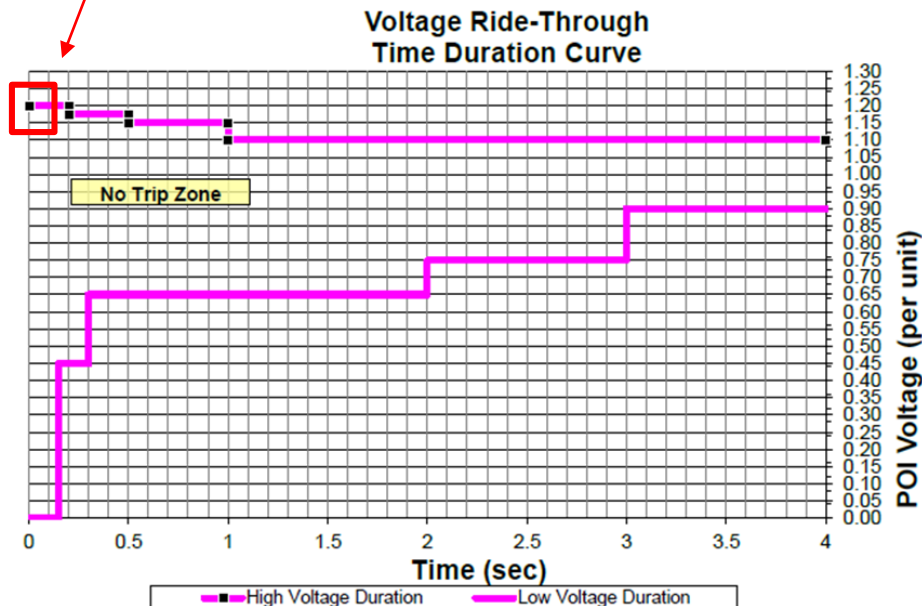
## Instantaneous voltage tripping and measurement filtering



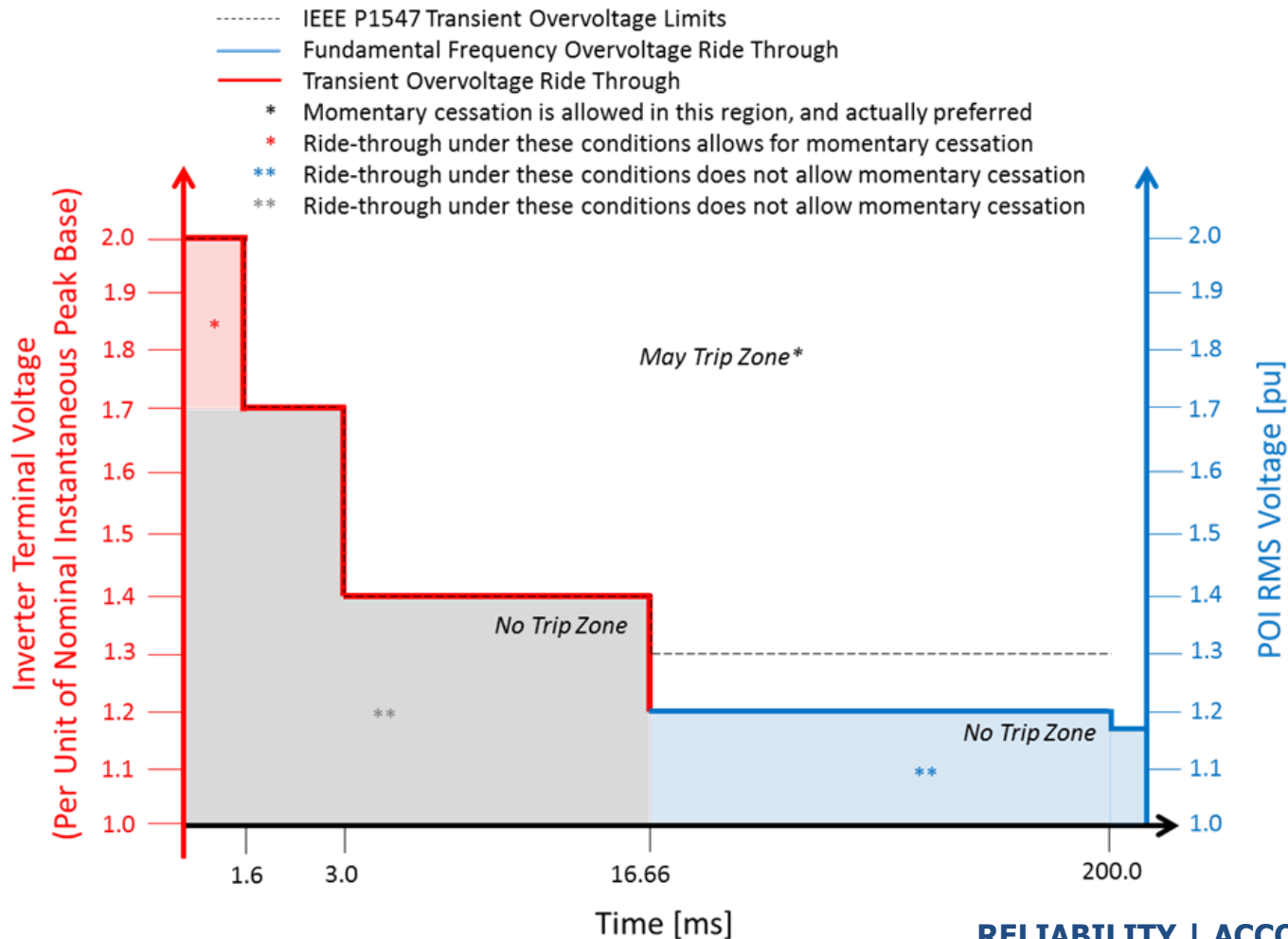
| Inst. Voltage [pu nominal peak] | Samples | Time [sec] | Cycles |
|---------------------------------|---------|------------|--------|
| > 1.1                           | 5       | 0.00167    | 0.1    |
| > 1.2                           | 4       | 0.00133    | 0.08   |
| > 1.3                           | 4       | 0.00133    | 0.08   |
| > 1.4                           | 3       | 0.00100    | 0.06   |

## Instantaneous voltage tripping and measurement filtering

| High Voltage Ride Through Duration |                    | Low Voltage Ride Through Duration |            |
|------------------------------------|--------------------|-----------------------------------|------------|
| Voltage (pu)                       | Time (sec)         | Voltage (pu)                      | Time (sec) |
| $\geq 1.20$                        | Instantaneous Trip | $\leq 0.45$                       | 0.15       |
| $\geq 1.175$                       | 0.20               | $\leq 0.65$                       | 0.30       |
| $\geq 1.15$                        | 0.50               | $\leq 0.75$                       | 2.00       |
| $\geq 1.10$                        | 1.00               | $\leq 0.90$                       | 3.00       |

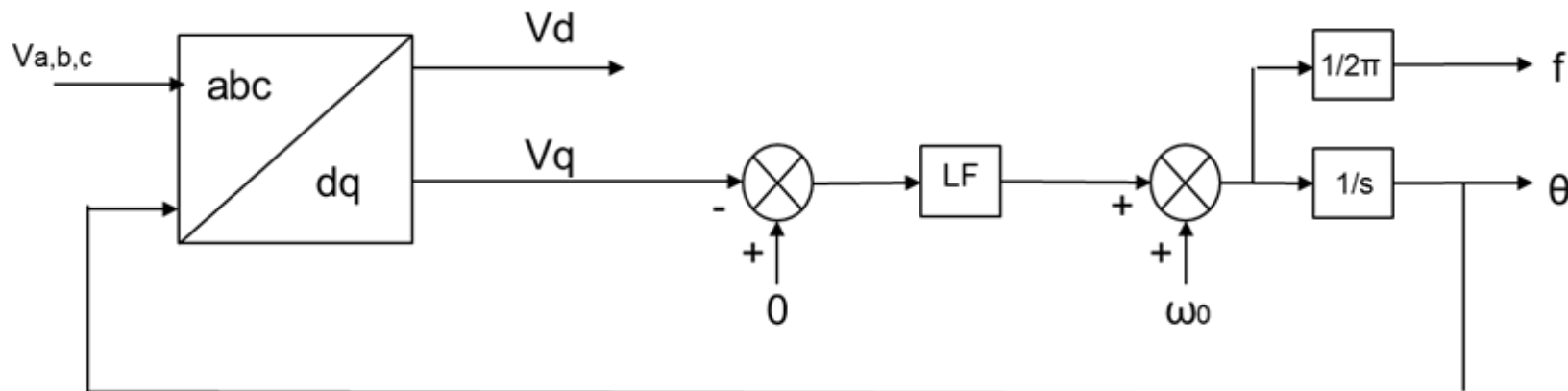


## Instantaneous voltage tripping and measurement filtering



## *Phase lock loop synchronization issues*

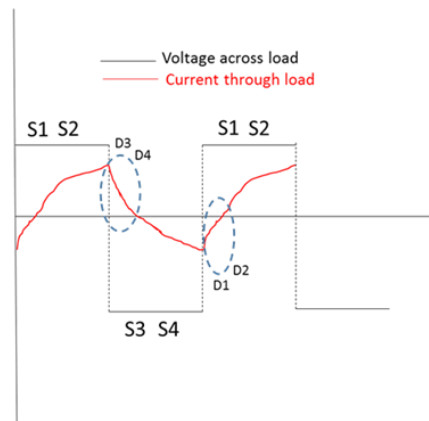
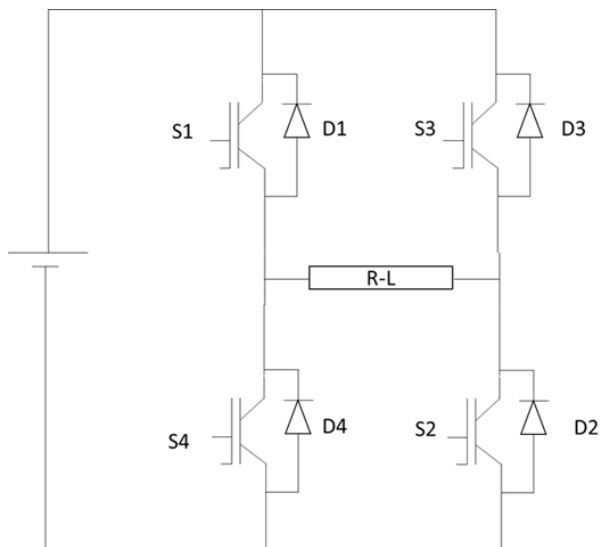
- Grid voltage phase jumps occur (e.g., during faults)
- Inverter PLLs should be robust to withstand BPS phase jumps
- Should not result in inverter tripping or momentary cessation
- Advanced controls should enable “PLL ride-through” rather than tripping





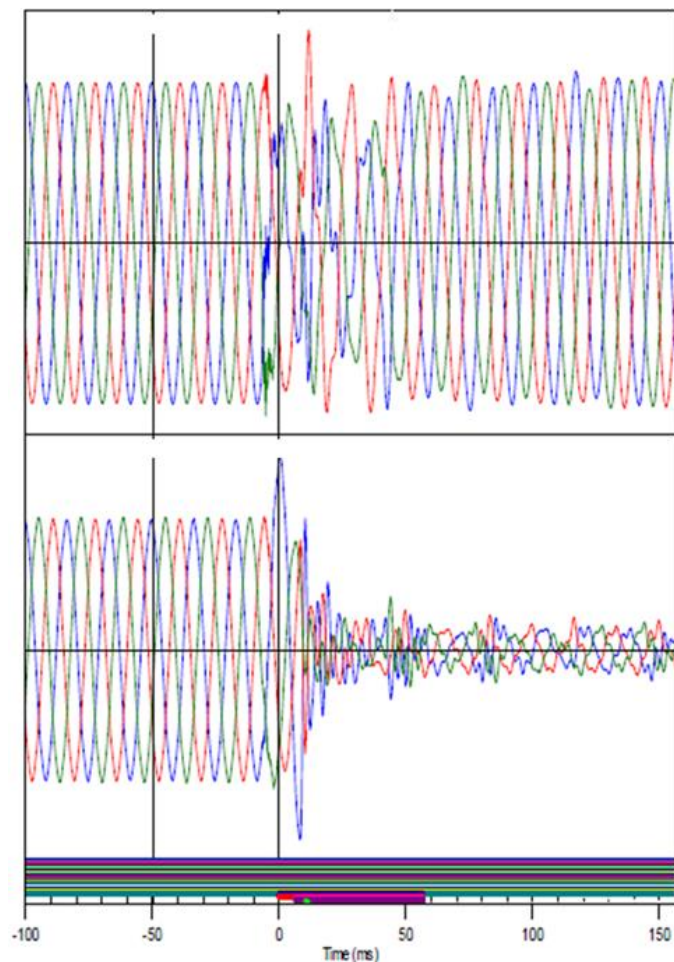
## *DC reverse current tripping*

- Anti-parallel diodes dissipate energy, mitigate voltage spikes
- Can conduct if forward biased (AC voltage > DC voltage)
- UL 1741 requires testing and detection, no specified trip settings
- DC reverse current detection protects panels, not inverter
- Very sensitive settings for one plant



## *Transient interactions and ride-through considerations*

- Interactions between momentary cessation, in-plant shunt capacitors, transient voltages, harmonics, etc., that are not sufficient understood
- Requires detailed electromagnetic transient (EMT) studies needed



- Disturbance Report to be published in February 2018
- NERC Alert to be published in likely March 2018
  - Mitigation of momentary cessation
  - Voltage protective control functions
  - PRC-024-2 curve interpretation
  - Transient overvoltage settings
- IRPTF will be publishing a Reliability Guideline on Inverter-Based Resources Performance in Q3 or Q4 2018

- Blue Cut Fire Disturbance Report:  
<http://www.nerc.com/pa/rrm/ea/Pages/1200-MW-Fault-Induced-Solar-Photovoltaic-Resource-Interruption-Disturbance-Report.aspx>
- EA Page (for future Disturbance Report):  
<http://www.nerc.com/pa/rrm/ea/Pages/default.aspx>
- NERC Alerts Page:  
<http://www.nerc.com/pa/rrm/bpsa/Pages/Alerts.aspx>
- IRPTF Page:  
<http://www.nerc.com/comm/PC/Pages/Inverter-Based-Resource-Performance-Task-Force.aspx>



# Questions and Answers

## **Rich Bauer**

Associate Director Reliability Risk Management-Event Analysis

Office (404) 446-9738

Cell (404) 357-9843

[rich.bauer@nerc.net](mailto:rich.bauer@nerc.net)

## **Ryan Quint**

Senior Manager, Advanced Analytics and Modeling

Office (202) 400-3015

Cell (202) 809-3079

[ryan.quint@nerc.net](mailto:ryan.quint@nerc.net)