NERC
NORTH AMERICAN ELECTRIC
RELIABILITY CORPORATION

Case Quality Metrics

Annual Interconnection-Wide Model Assessment

November 2023

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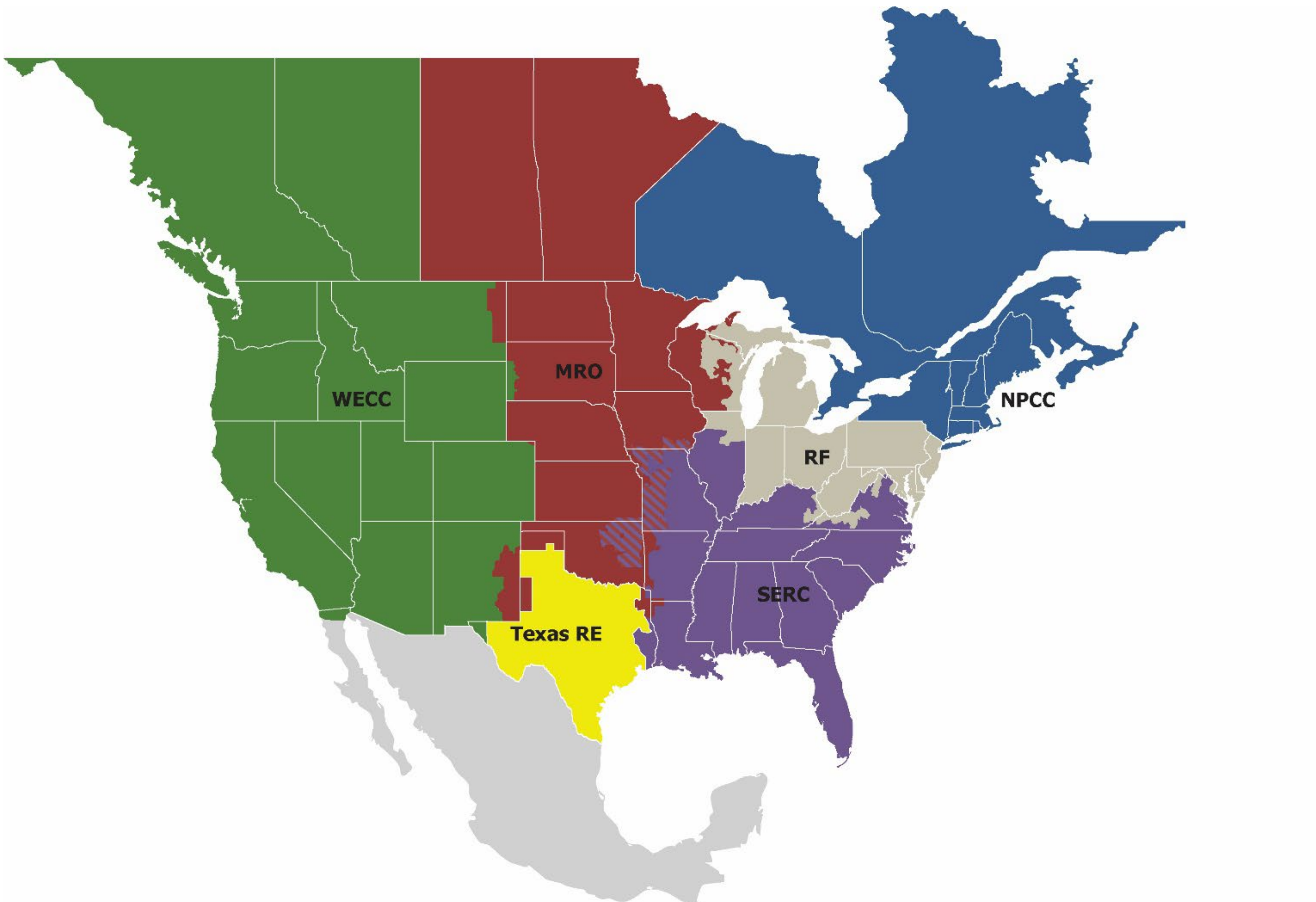
Preface

Electricity is a key component of the fabric of modern society and the Electric Reliability Organization (ERO) Enterprise serves to strengthen that fabric. The vision for the ERO Enterprise, which is comprised of NERC and the six Regional Entities, is a highly reliable, resilient, and secure North American bulk power system (BPS). Our mission is to assure the effective and efficient reduction of risks to the reliability and security of the grid.

Reliability | Resilience | Security
Because nearly 400 million citizens in North America are counting on us

The North American BPS is made up of six Regional Entities as shown on the map and in the corresponding table below. The multicolored area denotes overlap as some load-serving entities participate in one Regional Entity while associated Transmission Owners/Operators participate in another.



MRO	Midwest Reliability Organization
NPCC	Northeast Power Coordinating Council
RF	ReliabilityFirst
SERC	SERC Reliability Corporation
Texas RE	Texas Reliability Entity
WECC	WECC

Executive Summary

Powerflow and dynamics phasor model cases are the foundation for many power system studies. Calculations of operating limits, planning studies, and performance analyses for various operating conditions all depend on mathematical representations of transmission topology, generation, and load. Case quality refers to the reasonableness of the data in the individual equipment models that comprise the Base Case for the characteristics and operating states desired for study. A reasonable model contains information that is mathematically correct, does not contain suspicious data entries in part or at a whole, and presumes that sufficient procedures are in place to ensure that the equipment models that have been provided are accurate representations of the physical equipment the models are meant to represent. This *2023 Case Quality Metrics: Annual Interconnection-Wide Model Assessment* provides an unbiased and technically justified review of the powerflow and dynamics cases created for Interconnection-wide modeling purposes for the Eastern Interconnection[1] (EI), Western Interconnection (WI), and Texas Interconnection (TI).

Based on the results of the *2023 Case Quality Metrics Assessment*, NERC has provided the following list of observations for the MOD-032 designees with recommendations on which metrics to focus on to help improve model quality for base cases developed in the future:

- **EI**: There is a significant improvement in generator reactive limit power factor. However, performance above 5% continues with no noticeable improvement for dynamics records, including unacceptable models, not recommended models, inconsistent time constants, unreasonable inertia constants, and unreasonable saturation factors.
- **TI:** There is a significant improvement in "Second Generation Renewable Model Parameterization" due to extensive efforts between TI and NERC to appropriately evaluate this metric. Otherwise, the TI performance remains consistent.
- **WI:** There is a significant improvement in overall performance. The number of metrics worsening or maintaining poor performance has decreased.
- The generator reactive capability curve check for the EI or TI remains at 0.00 due to the lack of provided generator curves. Furthermore, no DER_A models[2] exist in the cases, and the DER_A tripping parameter check is still 0.00 for that reason.
- A majority of the metrics are below 5% while some are improving year-over-year as conversations between NERC and the MOD-032 designees continue.

Table ES.1 gives a "scorecard" for performance based on the overall assessment of cases for each Interconnection. Some metrics flag data that is more sensitive[3] to a study's results than others; however, each metric has similar weight for determining model quality. One of NERC's goals is to collaboratively improve model quality via various initiatives while working with MOD-032 designees, utility members, and subject matter experts. It is not intended for the metrics to have a 0% in all instances as legitimate modeling differences exist; however, these are uncommon and should not be prevalent in the Base Case. For this report, the performance is evaluated so that a higher percentage signifies more records flagged in the metric, and the goal is to trend towards 0%. The scorecard colors represent those trends.

[1] The Quebec Interconnection is included in these model builds and is represented by the EI MOD-032 designees.

[2] That is, in the generator tables.

[3] For example, some metrics flag conditions that will prevent dynamic initialization and thus prevent dynamic stability simulations. This influences dynamic stability results more than the Erroneous Power Development Fractions metric. Both are important to improving Interconnection-wide Base Case quality.

Based on the observations listed in **Table ES.1**, this report provides direct recommendations to each respective Interconnection's MOD-032 designee. The general recommendation is to continue tracking this year-over-year assessment and improve the metrics by engaging relevant subject matter experts.

Table ES.1: Interconnection Scorecard

Interconnection	Metrics	Evaluation
Eastern	Powerflow	Most metrics below 5% 1 metrics worsening, or consistent high score 1 metrics improving Voltage schedule conflicts increase
	Dynamics	Most metrics below 5% 4 metrics improving 7 metrics consistent high score 2 metric worsening
Texas	Powerflow	Most metrics below 5% 1 metrics improving 1 metric consistent high score 2 metric worsening
	Dynamics	Most metrics below 5% 2 metric improving 5 metrics consistent high score 2 metrics worsening
Western	Powerflow	Most metrics below 5% 4 metrics consistent high score 1 metrics improving 3 metrics worsening
	Dynamics	Most metrics below 5% 8 metrics consistent high score 4 metrics worsening 2 metrics improving,

Chapter 1: Background

A powerflow case is a collection of steady-state models for system topology, load, generation, dispatch, and interchange that constitute a snapshot of the selected set of operating conditions. A dynamics case is a collection of dynamic models used in conjunction with a powerflow case to perform a stability analysis of system performance.

This *2023 Case Quality Metrics Assessment* tracks the quality of the base cases created by the MOD-032 designees for the purposes of Interconnection-wide modeling and subsequent system studies. The assessment reviews each of the major Interconnections (i.e., EI,[4] WI, and TI). NERC works with the MOD-032 designees to select appropriate near-term Base Cases for each assessment. Trending the metrics provides an objective trend of Base Case quality by using technically justified metrics.

Base case quality has two principal aspects:

- **Case Data Quality:** Reasonableness of the data in the individual equipment models that comprise the case for the characteristics and operating states desired
- **Case Fidelity:** The ability of the case to accurately model measured power system behavior for the following details:
    - The type of system conditions the case is intended to model, such as heavy summer loads, light loads
    - The conditions measured during a distinct system event or disturbance

The metrics focus solely on the case data quality of the individual component models that comprise the Base Case. Validation of case fidelity or overall model performance requires comparison of the cases to actual measured system conditions and are not included in this report. Planning Coordinators are encouraged to consider these metrics in their MOD-033 evaluation and to also include metrics on case fidelity.

[4] The EI powerflow and dynamics cases include the Québec Interconnection.

Chapter 2: Case Quality Metrics

NERC has developed the following metrics that have vetted by industry through engagement with relevant subject matter experts and previous industry stakeholder committees.[5] The metrics are divided between steady-state and dynamics to characterize what type of study the metric is most relevant for checking case data quality. The metrics are updated annually by the NERC Advanced System Analytics and Modeling group. This process will change for future assessments to reflect appropriate oversight given the evolving ERO committee structure.

Steady-State Powerflow Metrics

The following list describes the steady-state powerflow metrics found under the heading **Metric Categorization** in **Table 2.1**. These descriptions are provided for those metrics applied to the powerflow data of the Interconnection-wide Base Case models. As the metrics change, the specific number assigned to each description may change as metrics are added or retired. The steady-state powerflow metrics are as follows:

- Dispatched generator real power output should not exceed the maximum real power capability of the unit ($P_{gen} <= P_{max}$). Note: Although small exceedances of this P_{max} rule appear trivial, the result is the same for all exceedances: the case will not initialize in dynamics.
- Dispatched generator real power output should not be less than the minimum real power capability of the unit ($P_{gen} >= P_{min}$). Note: Although small exceedances of this P_{min} rule appear trivial, the result is the same for all exceedances: the case will not initialize in dynamics.
- Scheduled area interchanges should sum to zero MW.
- Active voltage control devices controlling the same bus should not have conflicting voltage regulation set points.
- Transformers controlling voltage should have a voltage bandwidth that is sufficiently large in relation to the tap step of the transformer. Voltage bandwidths that are too small (or tap steps that are erroneously too large) may result in the lack of existence of a powerflow solution. The ratio of tap step (p.u.) to voltage bandwidth (p.u.) should be no less than 1.6; ratios below 1.0 are considered severe as they are extremely likely to prevent a powerflow solution from being found.[6]
- The continuous (Rate A) and emergency (Rate B) ratings of a branch should be consistent. The continuous rating (Rate A) of the branch circuit should be less than or equal to the emergency rating (Rate B), and the ratio between the emergency rating (Rate B) and the continuous rating (Rate A) is checked against a threshold value (3.0) to identify probable errors. Selection of this ratio is based on engineering judgment.
- Branch circuit loading should not exceed the circuit's continuous rating (Rate A): 100% of Rate A is used to identify exceedances; 105% of Rate A is used to identify severe exceedances.
- Generator reactive power output should not be dispatched at Q_{max} or Q_{min} (if $Q_{max} \neq Q_{min}$).[7]
- Generator reactive power limits (Q_{max} and Q_{min}) should have reasonable power factor[8] compared with maximum active power (P_{max}) within +0.80 (producing Vars) and -0.85 (consuming Vars).
- Parallel transformers should not have positive sequence circulating current.[9]

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[5] Such as the legacy NERC Planning Committee and the NERC Systems Analysis and Modeling Subcommittee

[6] This metric was changed in the *2017 Case Quality Metrics Assessment* from thresholds of 2 and 1.25 for normal and severe thresholds, respectively, to 1.6 and 1.0.

[7] Wind machines and units with $P_{gen} <= 0$ will be omitted from this check.

[8] Generators with $P_{max} = 0$ will be omitted to skip synchronous condensers.

[9] Opposite direction of positive sequence current flow

- Individual aggregate loads greater than 2 MVA[10] and with positive active and reactive power consumption[11] should have a power factor with absolute value greater than 0.5 pf.
- The ratio of generator R_{source}: X_{source} should be less than 1.0.[12]
- Generator terminal bus voltages should be between 0.95 and 1.05 when regulating a non-terminal bus.[13]
- For all generator capability curves provided, no part of the piecewise function can limit a box defined by the P_{max}, P_{min}, Q_{max}, Q_{min} box. A sample figure of a correctly constructed piecewise function is in **Figure 2.1** where the green box is not limited by the black curve.

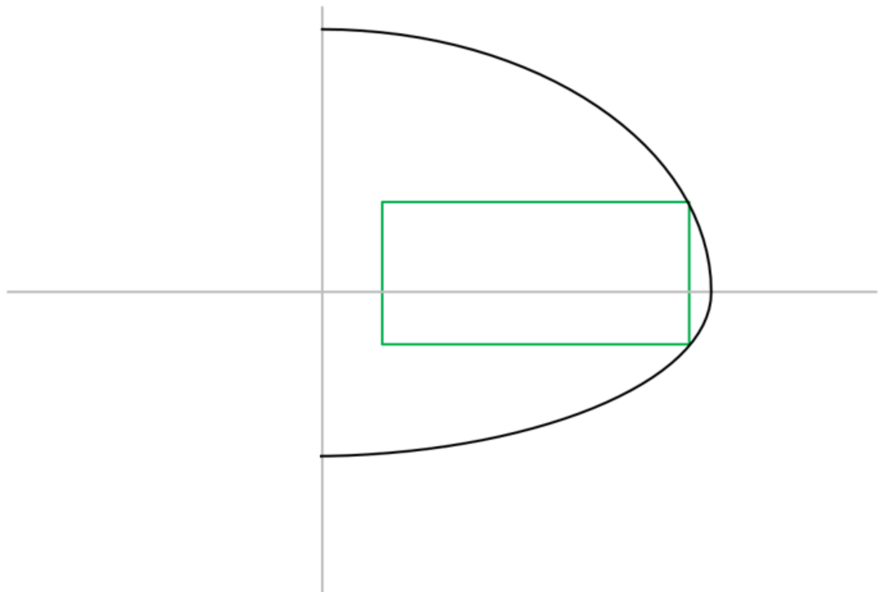

Figure 2.1: Generator Reactive Capability Box Overview

- All non-jumper transformers should have an X/R ratio between 5 and 2,000, and transmission lines should have an X/R ratio of less than 100. Exclusions include resistances with a value of zero and when reactance or resistance is less than zero.
- All natural gas generators in seasonal cases should change their maximum power available due to their relationship to ambient temperature conditions. All summer P_{max} values should be less than the winter P_{max} values.

Transient Dynamics Metrics

Continuing on from the steady-state metrics are the transient dynamics metrics. The numbers here continue as part of the entire set of metrics applied to the Interconnection-wide base cases and focus on the dynamics portion of data provided in such cases. Hence, the numbered list does not restart at 1. Some of these metrics require both powerflow and dynamic data to be loaded in the software in order to check the quality of the data and, as such, require longer processing time for larger data sets, indicated as follows:

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[10] This threshold is used to omit small loads that have little impact on the performance of the model; the focus is on pf of larger loads.
[11] This avoids shunt capacitor issues (negative reactive power) and net generators (negative active power value) represented in the load values.
[12] Except for X_{source} = 9999
[13] Non-synchronous devices are excluded from this check.

- Generating units larger than the criteria threshold established for each Interconnection[14] should have a generator model included in their dynamics record; units without a generator model are flagged as not meeting this modeling criteria.
- Generating units larger than the criteria threshold established for each Interconnection and that have a model (but are load netted anyway) are also tallied. This additional metric is needed to help identify all generating units without active models in the case as Item 17 overlooks generators that have models but are load netted anyway, and Item 19 below overlooks generators that lack models and are dispatched out-of-service in the case.
- Generating units larger than the criteria threshold established for each Interconnection should not be netted as negative load; any such units that are netted are flagged.
- Generating units larger than the criteria threshold established for each Interconnection[15] should not be modeled with a classical generator model.
- User written model penetration is also tallied for use in the MOD-032 case creation process.
- Generating units should have consistent generator reactance values. For example, the following measures are used to assess consistency of round rotor generators:
  - D-axis synchronous reactance (X_d) should not be less than d-axis transient reactance (X_d').
  - D-axis transient reactance (X_d') should not be less than d-axis subtransient reactance (X_d'').
  - Subtransient reactance (X_d'') should not be less than stator leakage reactance (X_l).
  - Q-axis synchronous reactance (X_q) should not be less than q-axis transient reactance (X_q').
  - Q-axis transient reactance (X_q') should not be less than q-axis subtransient reactance (X_q'').
- Generator time constants should be consistent: $T''_{d0} \leq T'_{d0}$ and $T''_{q0} \leq T'_{q0}$ [16] and $T'_{q0} \leq T'_{d0}$.[17]
- Generator inertia constants should be within reasonable ranges: $1.5 \leq H \leq 9.0$ for all generators greater than 20 MVA, and $1.0 \leq H \leq 10.0$ for machines less than 20 MVA.[18]
- Saturation factors S (1.0) and S (1.2) should be reasonable:[19]
  - $0.03 \leq S(1.0) \leq 0.18$
  - $0.2 \leq S(1.2) \leq 0.85$
  - S(1.2) should be within 2 to 8 times S(1.0).
  - Severe saturation factor check:
    - S(1.0) and S(1.2) should be greater than zero.
    - S(1.0) and S(1.2) should be less than 1.0.
    - S(1.0) should be less than or equal to S(1.2).
- Units with a power system stabilizer (PSS) should have an excitation system model.

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[14] 20 MVA for the EI; 10 MVA for the WI and TI

[15] 50 MVA for the EI and TI; 0 MVA for the WI

[16] GENTPJ (and gentpf in PSLF) has an exception to these rules since a salient pole machine is represented with$T'_{q0} = 0$. For this case, the only check used is $T''_{d0} \leq T'_{d0}$.

[17] This check is not applied to GENSAL and GENSAE generator models.

[18] These ranges were adopted based on industry feedback on the *2017 Case Quality Metrics Assessment*.

[19] This metric was changed in the *2017 Case Quality Metrics Assessment* from an S (1.0) maximum of .12 to .18 and an S (1.2) maximum of .80 to .85.

- Generator speed damping coefficient should be equal to zero for non-classical machine models.
- Turbine-governor models should have lead-time constants less than lag time constants.[20]
- Turbine power development fractions should add up to 1.0.[21] An example of these fractions in the block diagrams for a turbine governor model is in **Figure 2.2**.

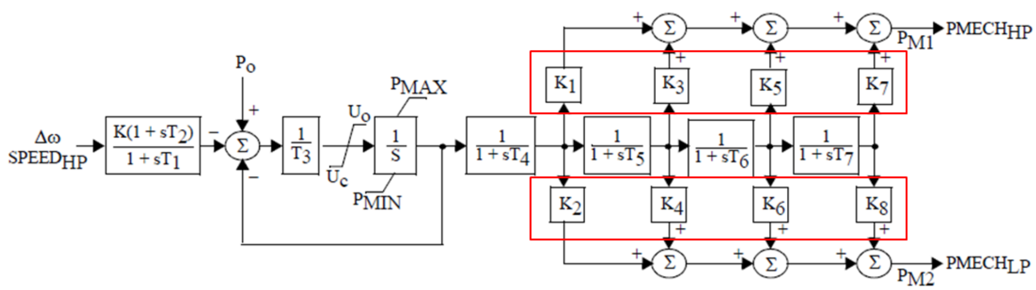

Figure 2.2: IEEEG1 Model Block Diagram (Source: Siemens PTI)

- DC exciter model self-excitation parameter K_E[22] should be a small negative number unless $K_E = 0$ (automatically calculated by program) or $K_E = 1$ (separately excited exciter). A sample block diagram for this parameter is highlighted in **Figure 2.3**.

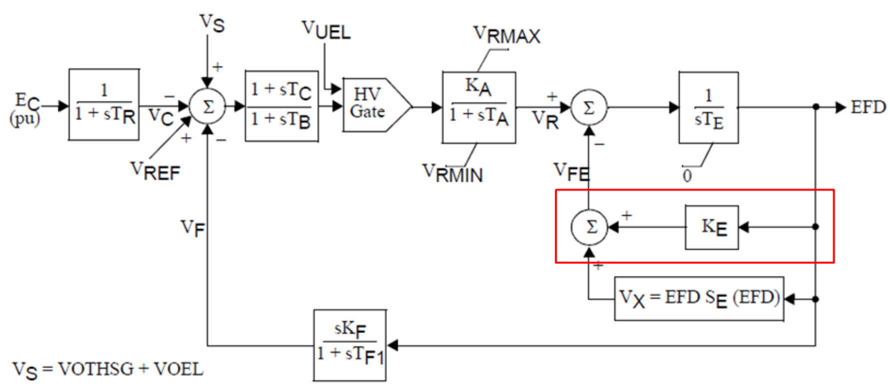

Figure 2.3: ESDC1A Model Block Diagram (Source: Siemens PTI)

- Wind turbine electrical model WT3E should have $\omega_{Pmin} < \omega_{P20} < \omega_{P40} < \omega_{P60} < \omega_{P100}$.
- PSS models should have reasonable parameters for the forward integration models. If Ks3 = 1, the parameters should be Ks1 > 0, $V_{stmax} > 0$, $V_{stmin} < 0$, Tw4 = 0, T7 = Tw2, T6 > 0.033, T8 = m*T9, and the input signals should be generator speed and generator electrical power. All such models that don't have these parameters or have Ks3 not equal to one are flagged for review. The PSS2A model, a forward integration PSS model, is found in **Figure 2.4**.

[20] This stabilizes the model as it reduces the forward path gain for high frequency changes in the input.

[21] This metric was corrected in the *2017 Case Quality Metrics Assessment* to check if K1+K2+K3+ . . . +K8 = 1.0.

[22] K_E reflects setting the shunt field rheostat for zeroing out the voltage regulator, often a small negative number.

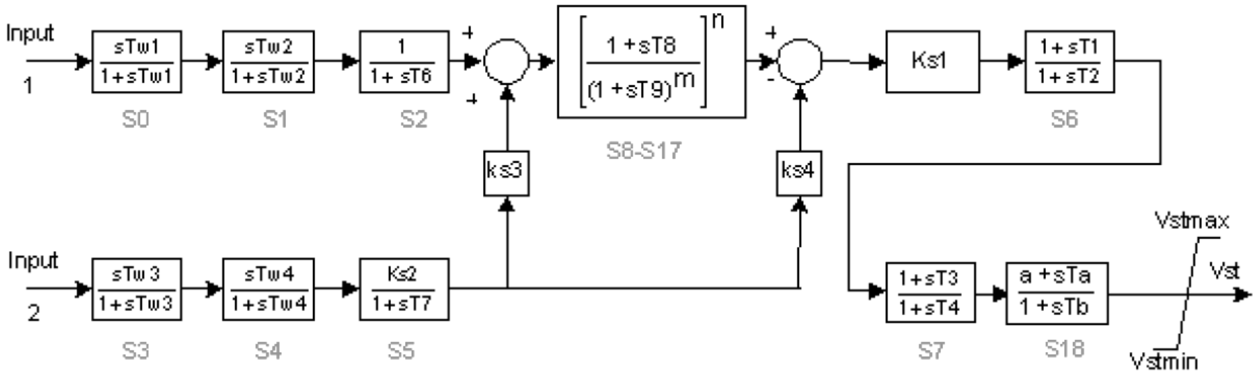

Figure 2.4: PSS2A Block Diagram [Source: GE PSLF]

- Models should not be listed as unacceptable or not recommended on the NERC Acceptable Model List:[23]
  - Unacceptable models are tallied for all generator, exciter, stabilizer, and turbine-governor models.
  - Not recommended models are tallied for all generator, exciter, stabilizer, and turbine-governor models.
- Second generation renewable models should be parameterized to site-specific conditions, namely as follows:
  - Renewable generator models (REGC) should have a difference between the “lvpnt0” and “lvpnt1” settings that are greater than 0.1 p.u.
  - REGCs should have a difference between the “zerox” and “brkpt” settings that are greater than 0.1 p.u.
  - REGCs should have a setting of “Tg” less than 0.2 seconds.
  - Renewable electrical models (REEC) should have a P_{max} setting of less than 1.0 p.u. of its dynamic MVA base.
  - REECs should have a Q_{max} setting of less than 1.0 p.u. of its dynamic MVA base.
  - REECs should have a Q_{min} setting of greater than -1.0 p.u. of its dynamic MVA base.
  - REECs should have a non-default K_{qv} setting.
  - REECs for battery energy storage systems should have a large Ts value.
    - It is a suspect condition for a “Ts” value under 1,000 seconds.
    - It is a severely suspect condition for a “Ts” value under 30 seconds.
  - Renewable plant models (REPC) should have a voltage control bus (or buses) and a monitored bus.
  - Wind turbine pitch controllers should not have identical parameters to another installation.

Metric Categorization

All of the case quality metrics are categorized by their impact to the Interconnection Base Case creation process in Table 2.1. These categorizations demonstrate how severe each metric is in impacting the data quality of the case. Metrics that are “bad data” are ones that find data that is blatantly incorrect. For example, reactance or time constant inconsistencies that are not physically possible. The term “suspect data” indicates data that looks abnormal and may or may not be in error. This should be reviewed by the MOD-032 designees more closely and addressed accordingly.

[23] All disclosures regarding ‘acceptability’ are documented in the spreadsheet on the Modeling Assessment Page here. If not listed on the spreadsheet, models are considered “acceptable.”

"Case setup issues" involve how individual elements are compiled (e.g., powerflow case or dynamics data file) and applied to create the initial operating state from which simulations would then be performed. Some metrics may have more than one indication of data (e.g., generators with a lack of modeling). These generators cannot be tracked in dynamics outside of load netting due to a lack of generator model, indicating a case setup issue. Since all Interconnections have a modeling threshold for explicit modeling, generators above that threshold also are suspect if they do not contain a dynamics model in the case.

Table 2.1: Bad and Suspect Data Metrics

Steady-State Metrics			
Metric	**Bad Data**	**Suspect Data**	**Case Setup Issue**
P_{max} Exceedances			X
P_{min} Exceedances			X
Scheduled Interchange Sum			X
Voltage Schedule Conflicts			X
Tap Step Conflicts		X	
Tap Step Conflicts (Severe)		X	
Low Emergency Rating		X	
High Emergency Rating		X	
Thermal Overloads			X
Thermal Overloads (Severe)			X
Gen Reactive at Limits			X
Gen Reactive Limit Power Factor		X	
Positive Sequence TX Circulating Current		X	
Poor Load Power Factor		X	
Generator R_{source}:X_{source} Ratio	X		
Generator Terminal Voltage			X
Generator Reactive Capability Curve		X	
X/R Ratio Check		X	
Natural Gas Generator P_{max}	X	X	
Gens without Models		X	X
Netted Gens with Models		X	X
Netted Generators		X	
Gens with Classical Models		X	
Unacceptable Models	X		
Not Recommended Models		X	
User-Written Models[24]		(X)	
Inconsistent Reactances	X		
Inconsistent Time Constants	X		
Unreasonable Inertia Constants		X	
Unreasonable Saturation Factors		X	
Severe Saturation Factors	X		
PSS but no Excitation		X	
Inconsistent Speed Damping	X		
Inconsistent Lead-Lag Time Constant	X		
Erroneous Power Dev Fractions	X		

[24] These are not affecting Interconnection performance. This is listed here based on discussions with MOD-032 designees.

Table 2.1: Bad and Suspect Data Metrics			
Steady-State Metrics			
Metric	Bad Data	Suspect Data	Case Setup Issue
DC Exciter Self-Excitation Errors	X		
Inconsistent Type III Wind Speeds	X		

Numerical Scores for Case Metrics

Generally, the raw count of each of the instances of data issues specified in the criteria above is not, by itself, a suitable metric. Most of these raw counts need to be scaled to reflect the size of the Interconnection being evaluated. This scaling is done by expressing each of the raw counts as a *percentage of the total number of elements* to which the corresponding criteria is applicable in the case. Each metric is reported as a count and performance is expressed as a percentage of all data issues identified[25] as a percentage of all applicable models.

Note that the denominator of the fractional values will differ for each metric tested based on the number of models under test. For example, the threshold values for applicable units may be different or the metric may relate to specific types of dynamic models.

Dynamics Cases

There are some specific qualifications on a few of the dynamic metrics that are noted in the following list:

- **Generators without models**: the number of generators meeting Interconnection size criteria for modeling with no dynamics model, expressed as a percentage of total number of generators (in-service and out-of-service), meeting Interconnection size criteria for modeling
- **Netted generators with models**: the number of generators meeting Interconnection size criteria for modeling with a dynamics model but load netted anyway, expressed as a percentage of total number of in-service generators meeting Interconnection size criteria for modeling
- **Netted generators**: the number of generators meeting Interconnection size criteria for modeling that are load netted and expressed as a percentage of total number of in-service generators meeting Interconnection size criteria
- **Generators with classical models**: the number of generators meeting Interconnection size criteria for non-classical modeling with a classical model expressed as a percentage of total number of generators (in-service and out-of-service) meeting Interconnection size criteria for non-classical modeling
- **Generators with faulty reactances**: the number of generators with inconsistent reactance data (e.g., $X_d'' < X_l$) expressed as a percentage of total number of generators (in-service and out-of-service) with models for which the reactance criteria is applicable (e.g., genrou, gentpj)

In addition, for each of the dynamic metrics, the maximum real and reactive power limits for each unit found to violate the criteria are totaled. When units were whitelisted by feedback from the MOD-032 designees, these sums were not altered; however, the percentage scores were altered. The total percentage is listed for all respective (generator, exciter, etc.) models in the case in terms of total number applicable for the check. For instance, a check that involves only generators will only check generator dynamic models.

[25] Generally, this is a one to one relationship with the number of models associated with an identified data issue.

Chapter 3: Software Differences and Considerations

Software Differences

Two software platforms are primarily used for assembling Interconnection-wide cases: Power Systems Simulator (PSS®E) from Siemens PTI (for the EI and TI) and Positive Sequence Load Flow (PSLF) from GE (for the WI). Because of differences in the handling of data by these two programs, the method for calculating the number of instances of criteria not being met may vary between Interconnections for some of the metrics. This is outlined in greater detail as follows:

PSS®E stores voltage set point for generators and static VAR systems with the device data record whereas PSLF stores voltage set point for these devices with the bus data record. In PSLF, it is not possible to have voltage schedule conflicts for multiple generators and static VAR systems that are regulating a common location. However, transformer data records in PSLF have their own voltage regulation data.

PSLF has a turbine type flag in the generator data to indicate if a generating unit is a wind unit.[26] However, this flag is not completely populated in WI base cases. Therefore, to eliminate wind units from the reactive limits check (Q_{gen} at Q_{max} or Q_{min}), the dynamics data file has to be loaded and the corresponding dynamic models have to be checked. The units with the any of the following wind generator models were eliminated from the check: genwri, gewtg, gewtgx, regc_a, regc_c, wt1g, wt2g, wt3g, and wt4g. It is recommended that the turbine type flag be utilized to improve the code's speed and complexity in identifying unit fuels.

The names of the dc exciter models differ between PSS®E and PSLF. Hence, for the check on parameter KE in dc exciters, the following models were checked in PSLF: esdc1a, esdc2a, esdc3a, esdc4b, exdc1, exdc2, exdc2a, exdc4, ieeet1, and rexs.

PSLF has the generator MVA base specified in both the powerflow and dynamics data files. All dynamic data is then taken on the per-unit MVA base specified in the dynamics data file. In PSS®E, one value of MVA base is specified and located in the powerflow file. In evaluating generator inertia constants for the WI base cases (using PSLF), the inertia constant evaluated on the MVA base specified in the powerflow file unless the specified powerflow base was the default 100 MVA. This calculated constant is an MVA base transfer between the dynamic and powerflow MVAs if the powerflow MVA is not 100 MVA.

Fuel types are not capable of being accessed in PSS®E. As such, for this current year's metrics, a N/A score is produced for the natural gas P_{max} check. Supplemental information may be required to check these cases for Interconnections that use PSS®E.

Other Considerations

In reading the data for a generator to determine its size, the generator MVA base value in the powerflow data record (MBASE) is not a reliable value to use for generator size since many small generators have the program default value of 100 MVA entered for this parameter. Therefore, a more comprehensive approach is used; generator MVA size is determined as the maximum value of the following:

- Dispatched MVA of the unit $\left(\sqrt{P_{gen}^2 + Q_{gen}^2}\right)$ where P_{gen} and Q_{gen} are the dispatched real and reactive output of the unit in the case
- MVA of the unit at maximum real and reactive limits $\left(\sqrt{P_{max}^2 + Q_{max}^2}\right)$ where P_{max} and Q_{max} are the maximum real and reactive output limits of the unit in the powerflow data

[26] For that matter, a variety of unit types can be specified and are used accordingly for multiple metrics.

- MBASE value unless value is 100.0 MVA (default value) in which case this parameter is ignored

Chapter 4: Case Quality Metric Assessment

The goal of the case quality metrics assessment is to promote good modeling practices and to strive to reduce data errors in Interconnection-wide base cases. Since the performance score is the percentage of elements that have data errors, the goal translates into attempting to drive performance scores towards zero. However, it is not expected that all performance scores reach zero. There are legitimate modeling reasons why some of the generic metrics developed by NERC in this 2023 Case Quality Metrics Assessment could be violated (e.g., equivalence or back-to-back dc ties between Interconnections). This information is provided to industry to gauge the quality of Interconnection-wide base cases for use in studies and assessments. A more detailed report is provided to the MOD-032 designees with the goal of assisting in improving the quality of the cases.

This assessment brings to light some of the modeling issues that have been identified by working with utility members, MOD-032 designees, and modeling groups in the electric utility industry. Some metrics serve to highlight more significant modeling errors that should be addressed directly. Other metrics serve to track modeling improvements that NERC is driving such as the Modeling Notifications Process developed by the NERC Systems Analysis and Modeling Subcommittee and now maintained by NERC staff.

The following subsections describe the performance scores for the assessment of each powerflow and dynamics case analyzed in the EI, TI, and WI. Note that performance scores greater than 5% are marked in **red**.

Notable Changes from Past Metrics

As the metrics are not infallible, many changes and alterations are supplied by industry to help gauge the quality Interconnection-wide base cases. Industry experts are able to send in suggestions and alterations to these metrics as the implementation of the scripts are posted alongside this report. Notable changes for TI in this report are the following:

Both the dynamic metrics scripts and TI excluded model list are updated after the extensive testing and discussion, which decrease the metrics on flagged warning for Second Generation Renewable Model Parameterization in Table 3.11, 3.14 and 3.17.

Change the Python script for all three interconnections prior to the performance of the 2024 CQM review to look for instances where the REPC model does not have a control bus or the cases where PPC is functionally disabled.

All concerns and python script changes will be discussed with MOD-32 Designees prior to the 2024 CQM review to insure that all changes will be applied in next year report.

Eastern Interconnection Case Quality Metrics Assessment

The performance and score, evaluated as a percentage, for all of the Eastern Interconnection cases are tabulated in **Table 4.1** to **Table 4.9**. **Table 4.1** to **Table 4.3** are for the 2023SUM Base Case; **Table 4.4** to **Table 4.6** are for the 2023WIN Base Case; **Table 4.7** to **Table 4.9** are for the 2023SLL Base Case.

EI 2023 Summer Peak Case: 2023SUM

Table 4.1: EI Steady-State Metrics 2023 Summer Peak Case: 2023SUM

Metric	Performance	Score (%)
Pmax Exceedances	25/7,219	0.35%
Pmin Exceedances	0/7,219	0.00%
Scheduled Interchange Sum	0.001	0.00%
Thermal Overloads (LOADING OVER RATE A)	229/101,967	0.22%
Thermal Overloads (Severe FLAGRANT LOADING OVER RATE A)	191/101,967	0.19%
Low Emergency Rating (RATE A > RATE B)	30/101,967	0.03%
High Emergency Rating (RATE B:RATE A RATIO TOO HIGH)	1/101,967	0.00%
Voltage Schedule Conflicts	412.0	-
Tap Step Conflicts	50/22,391	0.22%
Tap Step Conflicts (Severe)	13/23,391	0.06%
Generator Reactive at Limits	687/4,366	**15.74%**
Generator Reactive Limit Power Factor	200/5,748	3.48%
Positive Sequence TX Circulating Current	0/2,682	0.00%
Poor Load Power Factor	8/51,963	0.02%
Generator Reactive Capability Curve	0/0	0.00%
Generator Rsource: Xsource Ratio	9/7,219	0.12%
X/R Ratio Check	211/94,961	0.22%
Generator Terminal Voltage	111/2,752	4.03%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.2: EI Dynamics Metrics 2023 Sum

Metric	Performance	Score (%)	P_{max} (MW)	Q_{max} (MVAR)
Generators without Models	264/7,127	3.70%	8990.1	3070.4
Generators with Classical Models	14/5,393	0.26%	6,969.0	3,805.0
Netted Generators	113/5,114	2.21%	3,889.7	1,078.6
Netted Gens with Models	6/5,114	0.12%	291.9	165.7
Inconsistent Reactance	42/3,475	1.21%	4,025.8	2,061.3
Unacceptable Models (total)	2,187/20,638	**10.60%**	-	-
Not Recommended Models (total)	3,435/20,638	**16.64%**	-	-
User-Written Models[1]	-	-	-	-

Table 4.2: EI Dynamics Metrics 2023 Sum				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Inconsistent Time Constants	4/3,710	0.11%	312	186
Unreasonable Inertia Constants	391/4,676	**8.36%**	27,502.6	18,932.1
Unreasonable Saturation Factors	447/3,710	**12.05%**	47,881.2	25,532.8
Severe Saturation Factors	36/3,710	0.97%	4,163.6	2,186.0
PSS but no Excitation	4/7,127	0.06%	127.40	196.00
Inconsistent Speed Damping	93/4,524	2.06%	6,298.6	3,102.0
Inconsistent Lead-Lag Time Constant	38/1,631	2.33%	9,519.8	4,067.7
Erroneous Power Dev Fractions	22/497	4.43%	4,911.1	2,521.2
DC Exciter Self-Excitation Errors	121/805	**15.03%**	3,858.4	2,652.8
Inconsistent Type III Wind Speeds	0/189	0.00%	0.0	0.0
Suspect PSS2A/2B parameters	311/1,981	**15.70%**	66,041.8	40,696.3
Incorrect DER_A Tripping Parameters	0/0	0.0	0.0	0.0
Second Generation Renewable Model Parameterization[2]	549/1,858	**29.55%**	-	-

Table 4.3: EI Unacceptable and Not Recommended Model Breakdown			
Category	**Subcategory**	**Performance**	**Score (%)**
Unacceptable Models	Generator	1021/6,863	**14.88%**
	Exciter	382/6,521	**5.86%**
	Stabilizer	187/2,848	**6.57%**
	Turbine Governor	597/4,406	**13.55%**
Not Recommended Models	Generator	3,004/6,863	**43.77%**
	Exciter	0/6,521	0.00%
	Stabilizer	0/2,848	0.00%
	Turbine Governor	431/4,406	**9.78%**
User Written Models*	Generator	-	-
	Exciter	-	-
	Stabilizer	-	-
	Turbine Governor	-	-

EI 2023 Winter Peak Case: 2023WIN

Table 4.4: EI Steady-State Metrics 2023 Winter Peak Case		
Metric	**Performance**	**Score (%)**
P_{max} Exceedances	10/6,427	0.16%
P_{min} Exceedances	0/6,427	0.00%
Scheduled Interchange Sum	0	-
Thermal Overloads (LOADING OVER RATE A)	167/102,581	0.16%
Thermal Overloads (Severe FLAGRANT LOADING OVER RATE B)	70/102,581	0.07%
Low Emergency Rating (RATE A > RATE B)	25/102,581	0.02%
High Emergency Rating (RATE B:RATE A RATIO TOO HIGH)	1/102,581	0.00%
Voltage Schedule Conflicts	427	-
Tap Step Conflicts	56/22,580	0.25%
Tap Step Conflicts (Severe)	13/22,580	0.06%
Generator Reactive at Limits	623/3,900	**15.97%**
Generator Reactive Limit Power Factor	170/4,914	3.46%
Positive Sequence TX Circulating Current	0/2,698	0.00%
Poor Load Power Factor	18/49,606	0.04%
Generator Reactive Capability Curve	0/0	0.00%
Generator R_{source}:X_{source} Ratio	4/6,427	0.06%
X/R Ratio Check	212/95,510	0.22%
Generator Terminal Voltage	128/2,520	4.89%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.5: EI Dynamics Metrics 2023–2024 Winter Peak Case: 2023WIN				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	298/7,263	4.10%	10,387.9	3,695.4
Generators with Classical Models	14/5,490	0.26%	6,969.0	3,805.0
Netted Generators	69/4,411	1.56%	3,375.6	1,334.8
Netted Gens with Models	5/4,411	0.11%	194.5	105.7
Inconsistent Reactances	44/3,475	1.27%	4,050.0	2,573.9
Unacceptable Models (total)	2,199/20,886	**10.53%**	-	-
Not Recommended Models (total)	3,445/20,886	**16.49%**	-	-
User-Written Models[1]	-	-	-	-
Inconsistent Time Constants	4/3,721	0.11%	1,705.2	820.0
Unreasonable Inertia Constants	391/4,667	**8.38%**	27,898.3	18,716.6
Unreasonable Saturation Factors	448/3,721	**12.04%**	49,365.7	25,389.7
Severe Saturation Factors	36/3,721	0.97%	4,231.4	2,158.7
PSS but no Excitation	4/7,263	**6.00%**	127.4	196.0

Table 4.5: EI Dynamics Metrics 2023–2024 Winter Peak Case: 2023WIN				
Metric	Performance	Score (%)	P_{max} (MW)	Q_{max} (MVAR)
Inconsistent Speed Damping	93/4,515	2.06%	6,397.8	3,013.5
Inconsistent Lead-Lag Time Constant	39/1,634	2.39%	9,664.1	3,995.7
Erroneous Power Dev Fractions	23/495	4.65%	5,044.5	2,599.3
DC Exciter Self-Excitation Errors	119/803	**14.82%**	3,823.4	2,624.8
Inconsistent Type III Wind Speeds	0/189	0.00%	0.0	0.0
Suspect PSS2A/2B parameters	314/1,987	**15.80%**	68,373.6	40,983.5
Incorrect DER_A Tripping Parameters	0/0	0.00%	0.0	0.0
Second Generation Renewable Model Parameterization	601/1,956	**30.73%**	-	-

Table 4.6: EI Unacceptable and Not Recommended Model Breakdown 2023 WIN			
Category	Subcategory	Performance	Score (%)
Unacceptable Models	Generator	1,022/6,965	**14.67%**
	Exciter	393/6,630	**5.93%**
	Stabilizer	187/2,861	**6.54%**
	Turbine Governor	597/4,430	**13.48%**
Not Recommended Models	Generator	3,017/6,965	**43.32%**
	Exciter	0/6,630	0.00%
	Stabilizer	0/2,861	0.00%
	Turbine Governor	428/4,430	**9.66%**
User Written Models*	Generator	-	-
	Exciter	-	-
	Stabilizer	-	-
	Turbine Governor	-	-

EI 2023 Spring Light Load Case: 2023LL

Table 4.7: EI Steady-State Metrics 2023 Spring Light Load: 2023SLL		
Metric	Performance	Score (%)
P_{max} Exceedances	6/5,369	0.11%
P_{min} Exceedances	1/5,369	0.02%
Scheduled Interchange Sum	0.01	-
Thermal Overloads (LOADING OVER RATE A)	36/101,577	0.04%
Thermal Overloads (Severe FLAGRANT LOADING OVER RATE A)	22/101,577	0.02%
Low Emergency Rating (RATE A > RATE B)	26/101,577	0.03%
High Emergency Rating (RATE B:RATE A RATIO TOO HIGH)	1/101,577	0.00%
Voltage Schedule Conflicts	392	-

Table 4.7: EI Steady-State Metrics 2023 Spring Light Load: 2023SLL		
Metric	**Performance**	**Score (%)**
Tap Step Conflicts	50/22,255	0.22%
Tap Step Conflicts (Severe)	13/22,255	0.06%
Generator Reactive at Limits	509/2,687	**18.94%**
Generator Reactive Limit Power Factor	169/3,802	4.45%
Positive Sequence TX Circulating Current	0/2,654	0.00%
Poor Load Power Factor	16/48,092	0.03%
Generator Reactive Capability Curve	0/0	0.00%
Generator R_{source}:X_{source} Ratio	4/5,369	0.07%
X/R Ratio Check	218/94,617	0.23%
Generator Terminal Voltage	109/1,784	6.11%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.8: EI Dynamics Metrics 2023 Spring Light Load				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Qmax (MVAR)**
Generators without Models	288/7,118	4.05%	9,479.2	3,090.5
Generators with Classical Models	14/5,380	0.26%	6,969.0	3,805.0
Netted Generators	83/3,391	2.45%	3,088.3	941.7
Netted Gens with Models	9/3,391	0.27%	194.5	105.7
Inconsistent Reactances	42/3,482	1.21%	4,028.1	2,037.3
Unacceptable Models (total)	2,200/20,540	**10.71%**	-	-
Not Recommended Models (total)	3,449/20,540	**16.79%**	-	-
User-Written Models[27]	-	-	-	-
Inconsistent Time Constants	4/3,728	0.11%	1,704.0	820.0
Unreasonable Inertia Constants	389/4681	**8.31%**	27,546.8	18,473.0
Unreasonable Saturation Factors	447/3,728	**11.99%**	47,669.1	25,237.6
Severe Saturation Factors	36/3,728	0.97%	4,167.7	2,163.6
PSS but no Excitation	4/7,118	0.06%	127.4	196.0
Inconsistent Speed Damping	91/4,529	2.01%	5,667.6	2,619.7
Inconsistent Lead-Lag Time Constant	38/1,623	2.34%	9,519.8	4,067.7
Erroneous Power Dev Fractions	22/497	4.43%	4,923.0	2,521.2
DC Exciter Self-Excitation Errors	121/807	**14.99%**	3,858.4	2,652.8
Inconsistent Type III Wind Speeds	0/189	0.00%	0.0	0.0
Suspect PSS2A/2B parameters	334/1,796	**16.90%**	67,001.9	40,442.4
Incorrect DER_A Tripping Parameters	0/0	0.00%	0.0	0.0

[27] These are not affecting Interconnection performance. This is listed here based on discussions with MOD-032 designees.

Table 4.8: EI Dynamics Metrics 2023 Spring Light Load				
Metric	Performance	Score (%)	P_{max} (MW)	Qmax (MVAR)
Second Generation Renewable Model Parameterization	518/1,814	**28.56%**	-	-

Table 4.9: EI Unacceptable and Not Recommended Model Breakdown 2023SLL			
Category	Subcategory	Performance	Score (%)
Unacceptable Models	Generator	1,022/6,830	**14.96%**
	Exciter	390/6,487	**6.01%**
	Stabilizer	187/2,836	**6.59%**
	Turbine Governor	601/4,387	**13.70%**
Not Recommended Models	Generator	3,021/6,830	**44.23%**
	Exciter	0/6,487	0.00%
	Stabilizer	0/2,836	0.00%
	Turbine Governor	428/4,387	**9.76%**
User Written Models*	Generator	-	-
	Exciter	-	-
	Stabilizer	-	-
	Turbine Governor	-	-

Texas Interconnection Case Quality Metrics Assessment

The performance and score, evaluated as a percentage, for all of the Texas Interconnection cases are tabulated in Table 4.10 to Table 4.18. Table 4.10 to Table 4.12 are for the 2025_SP_Final_NonCnv Base Case; Table 4.13 to Table 4.15 are for the 2026_HWLL_Final_NonCnv Base Case; Table 4.16 to Table 4.18 are for the 2029_SP_Final_NonCnv Base Case.

TI 2025Summer Peak Case: 2025_SP_Final_NonCnv

Table 4.10: TI Steady-State Metrics: 2025_SP_Final_NonCnv

Metric	Performance	Score (%)
P_{max} Exceedances	0/1199	0.00%
P_{min} Exceedances	0/1199	0.00%
Scheduled Interchange Sum	0	0.00%
Thermal Overloads	28/11807	0.24%
Thermal Overloads (Severe)	22/11,807	0.19%
Low Emergency Rating	0/11,807	0.00%
High Emergency Rating	1/11,807	0.01%
Voltage Schedule Conflicts	47	-
Tap Step Conflicts	0/2017	0.00%
Tap Step Conflicts (Severe)	0/2017	0.00%
Generator Reactive at Limits	115/589	**19.52%**
Generator Reactive Limit Power Factor	103/1115	**9.24%**
Positive Sequence TX Circulating Current	0/49	0.00%
Poor Load Power Factor	0/5,776	0.00%
Generator R_{source}:X_{source} Ratio	0/1199	0.00%
X/R Ratio Check	36/9,809	0.37%
Generator Terminal Voltage	0/570	0.00%
Generator Reactive Capability Curve	0/0	0.00%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.11: TI Dynamics Metrics: 2025_SP_Final_NonCnv

Metric	Performance	Score (%)	P_{max} (MW)	Q_{max} (MVAR)
Generators without Models	48/1,267	3.79%	5516	3285
Generators with Classical Models	10/1,015	0.99%	4,824	4,492
Netted Generators with Models	0/1,134	0.00%	0	0
Netted Generators	1/1,134	0.09%	30	14.66
Inconsistent Reactances	6/407	1.47%	573	365
Unacceptable Models (total)	24/1,219	1.97%	-	-
Not Recommended Models (total)	443/1,219	**36.34%**	-	-

Table 4.11: TI Dynamics Metrics: 2025_SP_Final_NonCnv				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
User-Written Models[28]	669/4056	16.49%	-	-
Inconsistent Time Constants	2/457	0.44%	53	42
Unreasonable Inertia Constants	56/469	**11.94%**	2,521	1,542
Unreasonable Saturation Factors	58/457	**12.69%**	7,996	4,126
Severe Saturation Factors	8/457	1.75%	626	357
PSS but no Excitation	1/1,267	0.08%	47	16
Inconsistent Speed Damping	4/459	0.87%	82	55
Inconsistent Lead-Lag Time Constant	0/272	0.00%	0	0
Erroneous Power Dev Fractions	6/62	**9.68%**	3056	963
DC Exciter Self-Excitation Errors	4/32	**12.50%**	491	240
Inconsistent Type III Wind Speeds	0/0	0.00%	0	0
Suspect PSS2A/2B parameters	68/358	**18.99%**	4,426	2,981
Incorrect DER_A Tripping Parameters	0/0	0.00%	0	0
Second Generation Renewable Model Parameterization	28/619	4.52%	-	-

Table 4.12: TI Unacceptable and Not Recommended Model Breakdown			
Category	**Subcategory**	**Performance**	**Score (%)**
Unacceptable Models	Generator	24/1,219	1.97%
	Exciter	10/1,104	0.91%
	Stabilizer	0/588	0.00%
	Turbine Governor	0/588	0.00%
Not Recommended Models	Generator	443/1,219	**36.34%**
	Exciter	0/1,104	0.00%
	Stabilizer	0/588	0.00%
	Turbine Governor	0/588	0.00%
User Written Models*	Generator	221/1,290	17.13%
	Exciter	180/1141	15.78%
	Stabilizer	65/627	10.37%
	Turbine Governor	203/998	20.34%

TI 2026 Light Load Case: 2026_HWLL_Final_NonCnv

Table 4.13: TI Steady-State Metrics: 2026_HWLL_Final_NonCnv		
Metric	**Performance**	**Score (%)**
P_{max} Exceedances	0/648	0.00%
P_{min} Exceedances	0/648	0.00%

[28] These are not affecting Interconnection performance. This is listed here based on discussions with MOD-032 designees. Further, the MOD-032 designee, TexasRE, allows User Written Models for the TI base cases.

Table 4.13: TI Steady-State Metrics: 2026_HWLL_Final_NonCnv		
Metric	**Performance**	**Score (%)**
Scheduled Interchange Sum	0	0.00%
Thermal Overloads	33/11,813	0.28%
Thermal Overloads (Severe)	28/11,813	0.24%
Low Emergency Rating	0/11,813	0.00%
High Emergency Rating	1/11,813	0.01%
Voltage Schedule Conflicts	117	117
Tap Step Conflicts	0/2008	0.00%
Tap Step Conflicts (Severe)	0/2008	0.00%
Generator Reactive at Limits	31/235	13.19%
Generator Reactive Limit Power Factor	37/567	**6.53%**
Positive Sequence TX Circulating Current	0/50	0.00%
Poor Load Power Factor	1/5,764	0.02%
Generator R_{source}:X_{source} Ratio	0/648	0.00%
X/R Ratio Check	36/9,810	0.37%
Generator Terminal Voltage	0/169	0.00%
Generator Reactive Capability Curve	0/0	0.00%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.14: TI Dynamics Metrics: 2026_HWLL_Final_NonCnv				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	46/1,260	3.65%	5384	3240
Generators with Classical Models	10/1,012	0.99%	4824	4492
Netted Generators with Models	0/587	0.00%	0	0
Netted Generators	0/587	0.00%	0	0
Inconsistent Reactances	6/407	1.47%	593	365
Unacceptable Models (total)	24/1,214	1.98%	-	-
Not Recommended Models (total)	443/1,214	36.49%	-	-
User-Written Models[29]	624/4034	15.47%	-	-
Inconsistent Time Constants	2/457	0.44%	53	42
Unreasonable Inertia Constants	56/469	**11.94%**	2,667	1,542
Unreasonable Saturation Factors	58/457	**12.69%**	8,573	4,126
Severe Saturation Factors	8/457	1.75%	648	357
PSS but no Excitation	1/1,260	0.08%	50	16
Inconsistent Speed Damping	4/459	0.87%	82	55
Inconsistent Lead-Lag Time Constant	0/272	0.00%	0	0

[29] These are not affecting Interconnection performance. This is listed here based on discussions with MOD-032 designees. Further, the MOD-032 designee, TexasRE, allows User Written Models for the TI base cases.

Table 4.14: TI Dynamics Metrics: 2026_HWLL_Final_NonCnv				
Metric	Performance	Score (%)	P_{max} (MW)	Q_{max} (MVAR)
Erroneous Power Dev Fractions	6/62	9.68%	3105	963
DC Exciter Self-Excitation Errors	4/32	12.50%	491	240
Inconsistent Type III Wind Speeds	0/0	0.00%	0	0
Suspect PSS2A/2B parameters	68/358	18.99%	4,740	2,182
Incorrect DER_A Tripping Parameters	0/0	0.00%	0	0
Second Generation Renewable Model Parameterization	28/613	4.57%	-	-

Table 4.15: TI Unacceptable and Not Recommended Model Breakdown			
Category	Subcategory	Performance	Score (%)
Unacceptable Models	Generator	24/1,214	1.98%
	Exciter	10/1,099	0.91%
	Stabilizer	0/586	0.00%
	Turbine Governor	0/586	0.00%
Not Recommended Models	Generator	443/1,214	36.49%
	Exciter	21/890	2.36%
	Stabilizer	0/586	0.00%
	Turbine Governor	0/586	0.00%
User Written Models*	Generator	186/1,284	14.49%
	Exciter	177/1135	15.59%
	Stabilizer	66/624	10.58%
	Turbine Governor	195/991	19.68%

TI 2029 Summer Peak Case: 2029_SP_Final_NonCnv

Table 4.16: TI Steady-State Metrics :2029_SP_Final_NonCnv		
Metric	Performance	Score (%)
P_{max} Exceedances	0/1,238	0.00%
P_{min} Exceedances	0/1,238	0.00%
Scheduled Interchange Sum	0	0.00%
Thermal Overloads	36/11,884	0.30%
Thermal Overloads (Severe)	25/11,884	0.21%
Low Emergency Rating	0/11,884	0.00%
High Emergency Rating	1/11,884	0.80%
Voltage Schedule Conflicts	48	-
Tap Step Conflicts	0/2022	0.00%
Tap Step Conflicts (Severe)	0/2022	0.00%
Generator Reactive at Limits	107/626	17.09%
Generator Reactive Limit Power Factor	108/1152	9.38%

Table 4.16: TI Steady-State Metrics :2029_SP_Final_NonCnv		
Metric	**Performance**	**Score (%)**
Positive Sequence TX Circulating Current	0/50	0.00%
Poor Load Power Factor	0/5,814	0.00%
Generator R_{source}:X_{source} Ratio	0/1,238	0.00%
X/R Ratio Check	36/9,876	0.36%
Generator Terminal Voltage	0/588	0.00%
Generator Reactive Capability Curve	0/0	0.00%
Natural Gas Generator Pmax	N/A	N/A
Natural Gas Generator Pmax (Severe)	N/A	N/A

Table 4.17: TI Dynamics Metrics: 2029_SP_Final_NonCnv				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	47/1,266	3.71%	*5,531	*3,271
Generators with Classical Models	10/1,016	0.98%	4,824	4,492
Netted Generators with Models	0/1,173	0.00%	0	0
Netted Generators	0/1,173	0.00%	0	0
Inconsistent Reactances	6/407	1.47%	573	365
Unacceptable Models (total)	24/1,219	1.97%	-	-
Not Recommended Models (total)	443/1,219	**36.34%**	-	-
User-Written Models[30]	669/4057	16.49%	-	-
Inconsistent Time Constants	2/457	0.44%	53	42
Unreasonable Inertia Constants	56/469	**11.94%**	2,521	1,542
Unreasonable Saturation Factors	58/457	**12.69%**	7,996	4,126
Severe Saturation Factors	8/457	1.75%	626	357
PSS but no Excitation	1/1,266	0.08%	47	16
Inconsistent Speed Damping	4/459	0.87%	82	55
Inconsistent Lead-Lag Time Constant	0/272	0.00%	0	0
Erroneous Power Dev Fractions	6/62	**9.68%**	3,056	963
DC Exciter Self-Excitation Errors	4/32	**12.50%**	491	240
Inconsistent Type III Wind Speeds	0/0	0.00%	0	0
Suspect PSS2A/2B parameters	68/357	**19.05%**	4,426	2,982
Incorrect DER_A Tripping Parameters	0/0	0.00%	0	0
Second Generation Renewable Model Parameterization	30/619	4.85%	-	-

[30] These are not affecting Interconnection performance. This is listed here based on discussions with MOD-032 designees. Further, the MOD-032 designee, TexasRE, allows User Written Models for the TI base cases.

* This total is not indicative of the units identified score as the score can be modified by whitelisted units. This sum indicates the total Pmax and Qmax of units that are flagged by the check rather than the subset of remaining units after the exempted models are removed.

Table 4.18: TI Unacceptable and Not Recommended Model Breakdown			
Category	**Subcategory**	**Performance**	**Score (%)**
Unacceptable Models	Generator	24/1,219	1.97%
	Exciter	10/1,105	0.90%
	Stabilizer	0/588	0.00%
	Turbine Governor	0/588	0.00%
Not Recommended Models	Generator	443/1,219	**36.34%**
	Exciter	0/1,105	0.00%
	Stabilizer	0/588	0.00%
	Turbine Governor	0/588	0.00%
User Written Models*	Generator	221/1,290	17.13%
	Exciter	179/1,142	15.67%
	Stabilizer	66/627	10.53%
	Turbine Governor	203/998	20.34%

*Due to how PSS®E distinguishes "user-written" models in their software, this number may be higher and alters based on version of the software. Further, the MOD-032 designee, TexasRE, allows User Written Models for the TI base cases.

Western Interconnection Case Quality Metrics Assessment

The performance and score, evaluated as a percentage, for all of the Western Interconnection cases are tabulated in Table 4.19 to Table 4.26. Table 4.19 to Table 4.21 are for the 23HS4a1 Base Case; Table 4.22 to Table 4.24 are for the 23HW3a1_22 Base Case; Table 4.25 to Table 4.26 are for the 23LS1a1 Base Case.

WECC 2023 Summer Peak Case: 22HS3Sa

Table 4.19: Steady-State Metrics: 2023 Heavy Summer: 23HS4a		
Metric	**Score (%)**	**Performance**
P_{max} Exceedances	0.31%	11/3,531
P_{min} Exceedances	0.37%	13/3,531
Scheduled Interchange Sum	0.00%	0
Voltage Schedule Conflicts	0.61%	63/10,355
Tap Step Conflicts	0.24%	25/10,355
Tap Step Conflicts (Severe)	0.02%	5/30,155
Low Emergency Rating	0.01%	2/30,155
High Emergency Rating	0.01%	4/30,155
Thermal Overloads	0.04%	14/32,225
Thermal Overloads (Severe)	0.01%	4/32,225
Generator Reactive at Limits	**5.52%**	90 of 1630

Table 4.19: Steady-State Metrics: 2023 Heavy Summer: 23HS4a		
Metric	**Score (%)**	**Performance**
Generator Reactive Limit Power Factor	**9.47%**	398 of 3,897
Positive Sequence TX Circulating Current	0.00%	0 of 1,900
Poor Load Power Factor	0.04%	3 of 7,716
Generator R_{source}:X_{source} Ratio	0.22%	11 of 4,926
Generator Terminal Voltage	6.67%	90 of 1,350
Generator Reactive Capability Curve	2.43%	15 of 618
X/R Ratio Check	0.21%	124 of 57,701
Natural Gas Generator Pmax	**77.10%**	633 of 821
Natural Gas Generator Pmax (Severe)	4.14%	34 of 821

Table 4.20: WI Dynamics Metrics 2023 Summer Peak Case: 23HS4Sa1				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	282/3,935	**7.17%**	112,799.0	102,136.8
Netted Generators with Models	9/4,018	0.22%	758.5	131.2
Netted Generators	83/2,868	2.89%	4,681.4	1,751.6
Generators with Classical Models	0/4,926	0.00%	0.0	0.0
Unacceptable Models (total)	310/11,951	2.59%	9,898.2	2,650.7
Not Recommended Models (total)	929/13,859	**6.70%**	69,950.3	34,735.4
User-Written Models[1]	2/31,035	0.01%	-	-
Inconsistent Reactances	114/3222	3.54%	2,617.7	1,757.7
Units with Inconsistent Time Constant	212/3,221	**6.58%**	4,471.5	2,339.8
Inconsistent Inertia Constants	285/3,221	**8.85%**	*14,837.3	*9,761.5
Unreasonable Saturation factors	487/3,221	**15.12%**	*27,337.2	*12,962.7
Severe Saturation Factors	157/3,221	**5.34%**	*4,170.4	*1,884.1
PSS with NO Excitation System model:	25/1,845	1.36%	1,013.3	506.0
Units with Bad Speed Damping:	212/3,221	**6.58%**	3,550.6	1,652.9
Units with Bad Lead Lag Time Constants	59/1,275	4.63%	3,866.6	1,751.7
Erroneous Power Dev Fractions	6/168	3.57%	774.7	324.5
DC Exciter Self-Excitation Errors	27/442	**6.11%**	1,221.6	544,8
Inconsistent Type III Wind Speeds	0/57	0.00%	0.0	0.0
Suspect PSS2A/2B Parameters	47/1,660	2.83%	29,493.2	12.607.4
Second Generation Renewable Model Parameterization	942/3735	**25.22%**	-	-

Table 4.21: Unacceptable and Not Recommended Model Breakdown			
Category	**Subcategory**	**Performance**	**Score (%)**
Unacceptable Models	Generator	92 of 4,926	1.87%
	Exciter	92 of 4,683	2.01%
	Stabilizer	56 of 0	2.94%
	Turbine Governor	70 of 2,442	2.87%
Not Recommended Models	Generator	742 of 4,926	**15.06%**
	Exciter	136 of 4,583	2.97%
	Stabilizer	0 of 1,908	0.00%
	Turbine Governor	51 of 2,442	2.09%
User Written Models	None	2 of 31,035	0.15%

WECC 2022–2023 Winter Peak Case: 23HW3a1_22

Table 4.22: Steady-State Metrics Winter Peak Case: 23HW3a1_22		
Metric	**Score (%)**	**Performance**
P_{max} Exceedances	0.48%	13 out of 2,690
P_{min} Exceedances	0.22%	6 out of 2,690
Scheduled Interchange Sum	0.00%	0
Voltage Schedule Conflicts	0.66%	68 out of 10,248
Tap Step Conflicts	0.26%	27 out of 10,248
Tap Step Conflicts (Severe)	0.05%	5 out of 10,248
Low Emergency Rating	0.02%	5 out of 29,925
High Emergency Rating	0.01%	2 out of 29,925
Thermal Overloads	0.10%	33 out of 31,945
Thermal Overloads (Severe)	0.06%	20 out of 31,945
Generator Reactive at Limits	**5.22%**	95 out of 1,821
Generator Reactive Limit Power Factor	**8.71%**	332 out of 3,812
Positive Sequence TX Circulating Current	0.00%	0 out of 1,878
Poor Load Power Factor	0.10%	7 out of 6,975
Generator R_{source}:X_{source} Ratio	0.23%	11 out of 4,835
Generator Terminal Voltage	**6.80%**	126 out of 1,853
Generator Reactive Capability Curve	0.35%	2 out of 579
X/R Ratio Check	0.20%	115 out of 57,764
Natural Gas Generator Pmax	**97.61%**	940 out of 963
Natural Gas Generator Pmax (Severe)	1.14%	11 out of 963

Table 4.23: Dynamics Metrics 2022–2023 Winter Peak Case: 23HW3a1_22				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	290 of 3,851	**7.53%**	23,927.4	23,927.4
Netted Generators with Models	2 of 3,913	0.05%	70.5	31.0
Netted Generators	63 of 2,167	2.91%	3,401.7	1,239.9
Generators with Classical Models	0 of 4,835	0/4835	0.0	0.0
Unacceptable Models (total)	312 of 11,702	2.67%	9,918.2	2,511.7
Not Recommended Models (total)	943 of 13,602	**6.93%**	73,582.8	39,093.0
User-Written Models[1]	2 of 28,800	0.01%	0.0	0.0
Inconsistent Reactances	112 of 3177	3.53%	2,812.5	1,383.2
Units with Inconsistent Time Constant	208 of 3,177	**6.55%**	4,378.8	2,163.3
Inconsistent Inertia Constants	186 of 3,177	**5.85%**	15,023.1	9,770.3
Inconsistent Saturation factors	374 of 3,177	**11.77%**	27,091.3	12,603.9
Flagrantly Inconsistent Saturation Factors	144 of 3,177	4.53%	4,163.8	1,901.2
PSS with NO Excitation System model:	20 of 1,863	1.07%	1,917.7	715.6
Units with Bad Speed Damping:	216 of 3,177	**6.80%**	3,309.6	1,258.2
Units with Bad Lead Lag Time Constants	38 of 1,248	3.04%	1,923.0	3,476.6
Erroneous Power Dev Fractions	6 of 165	3.64%	774.7	324.5
DC Exciter Self-Excitation Errors	27 of 468	**5.77%**	1.227.7	518.3
Inconsistent Type III Wind Speeds	0 of 8	0.00%	0.0	0.0
Suspect PSS2A/2B Parameters	49 of 1,663	2.95%	30,229.3	13,115.9
Incorrect DER_A Tripping Parameters	0 of 0	0.00%	N/A	N/A
Second Generation Renewable Model Parameterization	912 of 2,387	**38.21%**	13,115.9	13,115.9

Table 4.24: Unacceptable and Not Recommended Model Breakdown; 2022–2023 Winter Peak Case: 23HW3a1			
Category	**Subcategory**	**Performance**	**Score (%)**
Unacceptable Models	Generator	93 of 4,835	1.92%
	Exciter	93 of 4486	2.07%
	Stabilizer	56 of 0	2.95%
	Turbine Governor	70 of 2,381	2.94%
Not Recommended Models	Generator	747 of 4,835	15.45%
	Exciter	145 of 4,486	3.23%

Table 4.24: Unacceptable and Not Recommended Model Breakdown; 2022–2023 Winter Peak Case: 23HW3a1			
Category	**Subcategory**	**Performance**	**Score (%)**
	Stabilizer	0 of 1,900	0.00%
	Turbine Governor	51 of 2,381	2.14%
User Written Models	DC Lines	2 of 28,800	0.17%

WECC 2023 Summer Light Load Case: 23LS1a

Table 4.25: Steady-State Metrics 2023 Summer Light Load Case: 23LS1a		
Metric	**Performance**	**Score (%)**
P_{max} Exceedances	0.28%	7 out of 2,457
P_{min} Exceedances	0.73%	18 out of 2,457
Scheduled Interchange Sum	0.00%	0
Voltage Schedule Conflicts	0.63%	65 out of 10,356
Tap Step Conflicts	0.26%	27 out of 10,356
Tap Step Conflicts (Severe)	0.05%	5 out of 10,356
Low Emergency Rating	0.01%	2 out of 30,160
High Emergency Rating	0.01%	4 out of 30,160
Thermal Overloads	0.02%	7 out of 32,227
Thermal Overloads (Severe)	0.02%	6 out of 32,227
Generator Reactive at Limits	3.76%	62 out of 1,651
Generator Reactive Limit Power Factor	**9.32%**	363 out of 3,893
Positive Sequence TX Circulating Current	0.00%	0 out of 1,904
Poor Load Power Factor	0.07%	4 out of 5,710
Generator R_{source}:X_{source} Ratio	0.22%	11 out of 4,927
Generator Terminal Voltage	**5.29%**	104 out of 1,966
Generator Reactive Capability Curve	0.00%	0 out of 457
X/R Ratio Check	0.21%	124 out of 58,327
Natural Gas Generator Pmax	**77.21%**	637 out of 825
Natural Gas Generator Pmax (Severe)	4.12%	34 out of 825

Table 4.26: Dynamics Metrics 2023 Summer Light Load Case: 23LS1a				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Generators without Models	283 of 3,937	**7.19%**	92,930.2	82,215.8
Netted Generators with Models	9 of 3,992	0.23%	137.0	131.2
Netted Generators	55 of 1,938	2.84%	3,697.3	1,736.2
Generators with Classical Models	0 of 4,927	0.00%	0.0	0.0
Unacceptable Models (total)	310 of 11,943	2.60%	9,898.2	2,653.7

Table 4.26: Dynamics Metrics 2023 Summer Light Load Case: 23LS1a				
Metric	**Performance**	**Score (%)**	**P_{max} (MW)**	**Q_{max} (MVAR)**
Not Recommended Models (total)	929 of 13,648	**6.81%**	69,950.3	34,848.0
User-Written Models[1]	2 of 27,275	0.01%	0.0	0.0
Inconsistent Reactances	114 of 3222	3.54%	2,617.7	1,757.7
Units with Inconsistent Time Constant	214 of 3,222	**6.64%**	4,552.5	2,394.6
Inconsistent Inertia Constants	332 of 3,222	2.27%	14,837.3	9,775.0
Inconsistent Saturation factors	534 of 3,222	**11.73%**	26,459.6	13,123.1
Flagrantly Inconsistent Saturation Factors	158 of 3,222	4.44%	4,170.4	1,947.4
PSS with NO Excitation System model:	18 of 1,841	0.98%	1,027.2	542.4
Units with Bad Speed Damping:	211 Of 3,222	**6.55%**	3,115.6	1,344.0
Units with Bad Lead Lag Time Constants	59 of 1,276	4.62%	3,866.6	1,745.3
Erroneous Power Dev Fractions	6 of 168	3.57%	774.7	324.5
DC Exciter Self-Excitation Errors	27 of 438	**6.16%**	1,221.6	520.2
Inconsistent Type III Wind Speeds	0 of 58	0.00%	0.0	0.0
Suspect PSS2A/2B Parameters	48 of 1,655	2.90%	29,557.3	12,579.6
Second Generation Renewable Model Parameterization	959 of 2,393	**40.08%**	0.0	0.0

Chapter 5: Observations

For the summer peak cases, **Table 5.1** demonstrates the number of metrics above 5% according to the categories identified in **Table 2.1**. Additional trending information between past NERC case quality metrics assessments and this year's version can be found in **Appendix A**.

Table 5.1: Interconnection Issues Categorized According to Table 1.1

Interconnection	Number of Bad Data Metrics above 5%	Number of Suspect Data Metrics above 5%	Number of Case Setup Issues above 5%
East	9	15	3
Texas	8	18	3
West	5	14	5

Based on the results of the case quality metrics assessment, the following observations are made:

- For EI, there is a significant improvement in the Generator Reactive Limit Power Factor. However for dynamics records including Unacceptable Models, Not Recommended Models, Inconsistent Time Constants, Unreasonable Inertia Constants, and Unreasonable Saturation Factors; performance above 5% continues with no noticeable improvement.
- For TI there is a significant improvement in the "Second Generation Renewable Model Parameterization" due to extensive efforts between TI and NERC to appropriately evaluate this metric. Otherwise, the TI performance remains consistent.
- For WECC there is a significant improvement in the overall performance. The number of metrics worsening or maintaining poor performance has decreased.
- The Generator Reactive Capability Curve check for the EI or TI remains at 0.00 due to the lack of provided generator curves. Further, no DER_A models[31] exist in the cases and the DER_A tripping parameter check is still 0.00 for that reason.
- A majority of the metrics are below 5% while some are improving year-over-year as conversations between NERC and the MOD-032 designees continue.
- WI has shown an improvement in the modeling of the severe saturation factor generators as requested in previous CQM Reports
- Generators dispatched at reactive limits remains an issue across the Interconnections. These generators in the Base Case are dispatched in a suspect manner.
- Generators with reactive limits that have relatively low power factor (i.e., large reactive limits relative to active power limits) are still an issue for the TI and WI Interconnections. The flagged data is suspected.
- Unreasonable inertia constants have improved significantly for TI and WI.
- Generator speed damping parameters with values other than zero are still an issue in the WI. Furthermore, a general trend towards improvement was made in the EI and TI.
- The dc exciter self-excitation errors are still an issue for all Interconnections. These generator models contain bad data.

[31] That is, in the generator tables.

- For WI, continued performance above the modeling 5% threshold for ***"***Generators without Models***"*** has been observed. The flagged generators indicate a case setup issue in addition to being a suspect condition for such generators.
- For EI, the Unacceptable Model metrics demonstrates a consistent performance above the 5% threshold. For all Interconnections, the Not Recommended Model metric is above 5%.

Table 5.2 gives a "scorecard" for performance based on the overall assessment of cases for each Interconnection. This performance is based on highlights from the specific observations above and the performance tables identified in **Appendix A**.

Table 5.2: Interconnection Scorecard

Interconnection	Metrics	Evaluation
Eastern	Powerflow	Most metrics below 5% 1 metrics worsening, or consistent high score 1 metrics improving Voltage schedule conflicts increase
	Dynamics	Most metrics below 5% 4 metrics improving 7 metrics consistent high score 2 metric worsening
Texas	Powerflow	Most metrics below 5% 1 metrics improving 1 metric consistent high score 2 metric worsening
	Dynamics	Most metrics below 5% 2 metric improving 5 metrics consistent high score 2 metrics worsening
Western	Powerflow	Most metrics below 5% 4 metrics consistent high score 1 metrics improving 3 metrics worsening
	Dynamics	Most metrics below 5% 8 metrics consistent high score 4 metrics worsening 2 metrics improving,

Chapter 6: Recommendations

Based on the previously listed observations, NERC recommends the following:

- NERC should continue performing the NERC case quality metrics assessment each year to assess the overall performance of case quality for the Interconnection-wide planning cases developed. NERC should then provide feedback to the MOD-032 designees for year-over-year improvement.
- NERC should continue working with subject matter experts to improve both the Powerflow and Dynamics metrics.
- The MOD-032 designees for the EI and TI should continue verifying the saturation factor curves and provide exceptions for verified generator parameters via a whitelist. The WI should focus on the severe saturation factor generators as a priority. Each MOD-032 designee should review the listed units with unreasonable saturation factors and work with their respective Generator Owners (GOs) to review model validation test reports to ensure accuracy.
- Generators above the modeling threshold for each Interconnection should have a model that conforms to the MOD-032 designees modeling practices (and all models should adhere to the NERC Acceptable Model List). The MOD-032 designees should review their model building process and enforce their modeling thresholds. The large majority of not recommended models is the generator model GENROU. MOD-032 designees are encouraged to read the *Modeling Notification:*
- The MOD-032 designees for each Interconnection should review the generators identified in the Generator Reactive Limit Power Factor to determine if the power factor is correct and provide verified exceptions via a whitelist.
- The MOD-032 designee for the WI should actively work with its GOs to correct units with inconsistent time constants. The metric is flagging generator model parameters that are not physically realistic.
- The MOD-032 designee for the WI should work with its respective GOs to correct the use of speed damping coefficients on units that are not modeled as classical machines. These values should be zero for generation units flagged.
- Each MOD-032 designee should work with their respective GOs to correct issues associated with the dc exciter self-excitation errors. This report provides some information in the description of the metric on how to correct these issues.
- The MOD-032 designees should ensure their natural gas generator thermal rates are represented in the Interconnection-wide base cases. When software inputs exist to determine fuel type, such fields should be filled out accordingly. Where such fields do not exist, supplemental data or requests to software venders should be made to encourage identification of generators with possibly large capacity changes due to ambient temperature. The MOD-032 designee for the WI should determine how feasible it is to request seasonal thermal limits in their ratings for natural gas generation facilities. The MOD-032 designees for the EI and TI should determine how to best include seasonal natural gas generator capacities into their base case packages.
- The MOD-032 designees should utilize the unacceptable and not recommended model generators adjusted for GENROU as flagged in those metrics to begin targeting efforts for model improvement and replacement.
- The MOD-032 designee for the WI should review their case cases to ensure that generator reactive capability curves are entered properly, that generator bus voltages stay within 0.95 and 1.05 p.u. and that generators are not dispatched to their reactive maximum capability.

- The MOD-032 designees for the WI and EI should ensure that the parameterization for second-generation renewable models is reflective of plant specific parameters. Generators flagged in the check have one or more models with parameters that are suspect.
- The MOD-032 designee for the WI should review their light summer cases to correct suspect generation data as more generation (as a percentage of all generators on-line) with suspect data seems to be used year-over-year.

Appendix A: Yearly Comparison

The metrics for each case were assessed to compare this year's performance against prior years' performance. The results of this assessment are shown in Tables A.1 to A.9. The color coding used in the tables denotes the following.

(dark green)	Consistent performance under 5% performance score, or performance score moved from greater than 5% to less than 5%
(light green)	Positive performance improvements (decrease in score of 2% or more from previous year)
(orange)	Continued performance above 5% performance score with no noticeable improvement
(red)	Noticeable performance degradation (increase of 1% or more from previous year), or performance score moved from less than 5% to greater than 5%

Figure A.1: Yearly Comparison Color Coding Chart

Many of the metrics are below 5% (dark green) signifying that the overall case quality of the Interconnection-wide base cases are consistently of good quality. Similar to Chapter 4, scores in **red** indicate a higher than 5% score for that year. A few metrics obtained light green scores indicating an improvement of case quality and the few scores that had the orange score, indicating a stable, but high score. It is good to note that the EI Base Case Creation Process has a series number associated with the Base Case that will not line up with the year listed in the tables. Thus, there is a year difference between the series number and the case quality metrics assessment year. To further clarify, the case quality metrics assessment year is X, and the EI builds their models for year X in year X-1.

Eastern Interconnection

Table A.1: EI Heavy Summer Cases

Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%)	Performance
Powerflow	P_{max} Exceedances	0.1	0.05	0.06	0.06	0.35%	(dark green)
	P_{min} Exceedances	0.1	0.02	0.01	0.01	0.00%	(dark green)
	Scheduled Interchange Sum	0.01	0	0	0	0.00%	(dark green)
	Thermal Overloads	0.19	0.13	0.15	0.19	0.22%	(dark green)
	Thermal Overloads (Severe)	0.15	0.11	0.12	0.15	0.19%	(dark green)
	Low Emergency Rating	0	0.02	0.02	0.03	0.03%	(dark green)
	High Emergency Rating	0	0	0	0.09	0.00%	(dark green)
	Voltage Schedule Conflicts	14	29	102	118	412	(red)
	Tap Step Conflicts	0.07	0.16	0.17	0.18	0.22%	(dark green)
	Tap Step Conflicts (Severe)	0.01	0.09	0.09	0.06	0.06%	(dark green)
	Generator Reactive at Limits	**18.88**	**16.52**	**15.7**	**16.42**	**15.74%**	(orange)
	Generator Reactive Limit Power Factor	**12.14**	**10.3**	2.38	**8.09**	3.48%	(light green)
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	(dark green)
	Poor Load Power Factor	0.29	0.3	0.33	0.44	0.02%	(dark green)
	Generator Reactive Capability Curve	0	0	0	0	0.00%	(dark green)

Table A.1: EI Heavy Summer Cases							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%)	Performance
	Generator R_{source}:X_{source} Ratio	0	0.06	0.04	0.11	0.12%	
	X/R Ratio Check	0.25	0.25	0.23	0.23	0.22%	
	Generator Terminal Voltage	**6.33**	**5.53**	4.15	4.07	4.03%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Generators without Models	1.96	2.26	2.37	2.98	3.70%	
	Generators with Classical Models	0.25	0.28	0.27	0.27	0.26%	
	Netted Generators with Models	0.64	0.47	0.37	2.51	2.21%	
	Netted Generators	2.65	2.79	2.48	0.18	0.12%	
	Inconsistent Reactance	0.24	0.82	1.05	1.06	1.21%	
	Unacceptable Models	**11.83**	**11.81**	**13.17**	**12.36**	**10.60%**	
	Not Recommended Models	**23.56**	**21.09**	**19.87**	**18.29**	**16.64%**	
	User-Written Models[32]	N/A	-	-	-	-	
	Inconsistent Time Constants	0.11	0.13	0.09	0.07	0.11%	
	Unreasonable Inertia Constants	**8.44**	**8.06**	**7.77**	**8.18**	**8.36%**	
	Unreasonable Saturation Factors	**10.76**	**11**	**11.09**	**12**	**12.05%**	
	Severe Saturation Factors	0.81	0.9	0.9	1.02	0.97%	
	PSS but no Excitation	0.06	0.1	0.06	0.06	0.06%	
	Inconsistent Speed Damping	3.13	2.22	2.28	2.52	2.06%	
	Inconsistent Lead-Lag Time Constant	2.06	1.82	1.9	1.94	2.33%	
	Erroneous Power Dev Fractions	1.27	1.2	3.48	3.81	4.43%	
	DC Exciter Self-Excitation Errors	**10.58**	**12.83**	**13.4**	**13.56**	**15.03%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**16.69**	**17.01**	**18.54**	**17.56**	**15.70%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0	
	Second Generation Renewable Model Parameterization	N/A	N/A	**17.57**	**21.87**	**29.55%**	

[32] Performance not tracked

Table A.2: EI Heavy Winter Cases							
Type of Metric	**Metric**	**2019 Score (%)**	**2020 Score (%)**	**2021 Score (%)**	**2022 Score (%)**	**2023 Score (%**	**Performance**
Powerflow	P_{max} Exceedances	0.1	0.02	0.03	0.02	0.16%	
	P_{min} Exceedances	0.16	0.02	0	0	0.00%	
	Scheduled Interchange Sum	0	0	0	0	-	
	Thermal Overloads	0.18	0.15	0.14	0.14	0.16%	
	Thermal Overloads (Severe)	0.14	0.12	0.11	0.11	0.07%	
	Low Emergency Rating	0	0.03	0.02	0.02	0.02%	
	High Emergency Rating	0	0	0	0	0.00%	
	Voltage Schedule Conflicts	16	36	107	118	427	
	Tap Step Conflicts	0.07	0.16	0.17	0.18	0.25%	
	Tap Step Conflicts (Severe)	0	0.09	0.09	0.06	0.06%	
	Generator Reactive at Limits	**17.99**	**14.48**	**17.01**	**16.77**	**15.97%**	
	Generator Reactive Limit Power Factor	**11.14**	**8.54**	2.46	**7.17**	3.46%	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.24	0.25	0.27	0.43	0.04%	
	Generator Reactive Capability Curve	0	0	0	0.05	0.00%	
	Generator R_{source}:X_{source} Ratio	0	0.05	0.05	0.16	0.06%	
	X/R Ratio Check	0.26	0.24	0.23	0	0.22%	
	Generator Terminal Voltage	**7.75**	4.5	**5.28**	4.13	4.89%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Gens without Models	2.07	2.39	2.59	3.21	4.10%	
	Gens with Classical Models	0.27	0.28	0.27	0.28	0.26%	
	Netted Generators	2.45	2.17	2.09	1.81	1.56%	
	Netted Generators with Models	0.71	0.26	0.34	0.21	0.11%	
	Inconsistent Reactance	0.27	0.64	1.1	1.05	1.27%	
	Unacceptable Models	**13.87**	**10.33**	**13.15**	**12.26**	**10.53%**	
	Not Recommended Models	**23.48**	**20.94**	**19.69**	**18.15**	**16.49%**	
	User-Written Models[1]	N/A	-	-	-	-	
	Inconsistent Time Constants	0.11	0.13	0.09	0.12	0.11%	
	Unreasonable Inertia Constants	**8.49**	**8.07**	**7.76**	**8.12**	**8.38%**	
	Unreasonable Saturation Factors	**10.75**	**10.99**	**11.12**	**11.95**	**12.04%**	
	Severe Saturation Factors	0.81	0.91	0.9	1.01	0.97%	
	PSS but no Excitation	0.06	0.1	0.06	0.06	**6.00%**	
	Inconsistent Speed Damping	3.12	2.22	2.28	2.51	2.06%	

Table A.2: EI Heavy Winter Cases							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	Inconsistent Lead-Lag Time Constant	2.16	1.81	1.88	1.93	2.39%	
	Erroneous Power Dev Fractions	1.27	1.2	3.48	3.77	4.65%	
	DC Exciter Self-Excitation Errors	**10.77**	**12.59**	**13.43**	**13.4**	**14.82%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**16.67**	**17.32**	**18.63**	**17.6**	**15.80%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	
	Second Generation Renewable Model Parameterization	N/A	N/A	**18.57**	**24.22**	**30.73%**	

Table A.3: EI Light Spring Cases							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0.06	0.17	0	0	0.11%	
	P_{min} Exceedances	0.21	0.11	0.05	0	0.02%	
	Scheduled Interchange Sum	0	0.001	0	0	-	
	Thermal Overloads	0.07	0.05	0.04	0.04	0.04%	
	Thermal Overloads (Severe)	0.06	0.05	0.03	0.03	0.02%	
	Low Emergency Rating	0	0.02	0.02	0.03	0.03%	
	High Emergency Rating	0	0	0	0	0.00%	
	Voltage Schedule Conflicts	13	38	70	117	392	
	Tap Step Conflicts	0.06	0.16	0.17	0.18	0.22%	
	Tap Step Conflicts (Severe)	0	0.09	0.09	0.07	0.06%	
	Generator Reactive at Limits	**20.87**	**19.64**	**16.98**	**18.56**	**18.94%**	
	Generator Reactive Limit Power Factor	**13.65**	**9.29**	2.44	**8.32**	4.45%	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.38	0.35	0.28	0.41	0.03%	
	Generator Reactive Capability Curve	0	0	0	0	0.00%	
	Generator R_{source}:X_{source} Ratio	0	0.08	0.08	0.15	0.07%	
	X/R Ratio Check	0.25	0.24	0.23	0.23	0.23%	
	Generator Terminal Voltage	**13.51**	**6.07**	**6.09**	**14.05**	**6.11%**	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Generators without Models	1.81	2.36	2.62	2.86	4.05%	

Table A.3: EI Light Spring Cases							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	Generators with Classical Models	0.23	0.28	0.26	0.27	0.26%	
	Netted Generators	2.75	2.06	2.21	2.12	2.45%	
	Netted Gens with Models	1.05	0.31	0.73	0.23	0.27%	
	Inconsistent Reactances	0.25	0.82	1.06	1.06	1.21%	
	Unacceptable Models	**13.95**	**11.86**	**13.23**	**17.59**	**10.71%**	
	Not Recommended Models	**23.79**	**21.15**	**19.95**	**48,00**	**16.79%**	
	User-Written Models[1]	N/A	-	-	-	-	
	Inconsistent Time Constants	0.11	0.13	0.09	0.07	0.11%	
	Unreasonable Inertia Constants	**8.32**	**8.01**	**7.8**	**8.18**	**8.31%**	
	Unreasonable Saturation Factors	**10.78**	**11.04**	**10.99**	**11.95**	**11.99%**	
	Severe Saturation Factors	0.81	0.91	0.91	1.02	0.97%	
	PSS but no Excitation	0.06	0.11	0.07	0.06	0.06%	
	Inconsistent Speed Damping	3.12	2.23	2.29	2.52	2.01%	
	Inconsistent Lead-Lag Time Constant	2.08	1.83	1.92	2.22	2.34%	
	Erroneous Power Dev Fractions	1.09	1.21	3.49	4.09	4.43%	
	DC Exciter Self-Excitation Errors	**10.58**	**12.84**	**13.45**	**13.57**	**14.99%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**17.73**	**18.09**	**19.55**	**18.85**	**16.90%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	
	Second Generation Renewable Model Parameterization	N/A	N/A	**17.31**	**21.63**	**28.56%**	

Texas Interconnection

Table A.4: TI Heavy Summer Peak Cases: 2025_SP_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0	0	0.11	0	0.00%	
	P_{min} Exceedances	0	0	0	0.08	0.00%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Thermal Overloads	0.06	0.1	0.24	0.25	0.24%	
	Thermal Overloads (Severe)	0.04	0.04	0.23	0.25	0.19%	
	Low Emergency Rating	0	0	0	0	0.00%	
	High Emergency Rating	0.03	0	0.02	0.02	0.01%	
	Voltage Schedule Conflicts	5	47	31	47	47	
	Tap Step Conflicts	0.07	1.33	3.66	3.57	0.00%	

Table A.4: TI Heavy Summer Peak Cases: 2025_SP_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	Tap Step Conflicts (Severe)	0	0	0	0	0.00%	
	Generator Reactive at Limits	**6.37**	**6.78**	**8.52**	**13.9**	**19.52%**	
	Generator Reactive Limit Power Factor	**13.73**	**31.83**	**9.36**	**9.3**	**9.24%**	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.13	0.06	0.02	0.05	0.00%	
	Generator R_{source}:X_{source} Ratio	0.13	0	0.42	0.62	0.00%	
	X/R Ratio Check	0.43	0.44	0.34	0.42	0.37%	
	Generator Terminal Voltage	1.92	0.3	0.58	0	0.00%	
	Generator Reactive Capability Curve	0	0	0	0	0.00%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Generators without Models	**5.2**	2.52	2.88	1.79	3.79%	
	Generators with Classical Models	2.15	0	1.22	1.09	0.99%	
	Netted Gens with Models	0	0	0	0.3	0.00%	
	Netted Generators	0	0	0	0.3	0.09%	
	Inconsistent Reactances	0.62	1.07	1.31	1.13	1.47%	
	Unacceptable Models	2.96	2.1	1.85	1.42	1.97%	
	Not Recommended Models	**24.37**	**21.77**	**20.09**	**17.08**	**36.34%**	
	User-Written Models[33]	N/A	-	-	-	**16.49%**	
	Inconsistent Time Constants	0.4	0.79	0.73	0.69	0.44%	
	Unreasonable Inertia Constants	**14.01**	**15.31**	**16.4**	**18.86**	**11.94%**	
	Unreasonable Saturation Factors	**13.17**	**12.82**	**13.55**	**13.13**	**12.69%**	
	Severe Saturation Factors	1.2	1.18	1.65	1.55	1.75%	
	PSS but no Excitation	0	0	0	0	0.08%	
	Inconsistent Speed Damping	3.1	2.82	2.91	2.92	0.87%	
	Inconsistent Lead-Lag Time Constant	0	0	0	0	0.00%	
	Erroneous Power Dev Fractions	0	0	2.44	**7.84**	**9.68%**	
	DC Exciter Self-Excitation Errors	**12.5**	**13.46**	**11.31**	**10.53**	**12.50%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**16.92**	**14.07**	**16.21**	**17.87**	**18.99%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	

[33] Performance not tracked.

Table A.4: TI Heavy Summer Peak Cases: 2025_SP_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	Second Generation Renewable Model Parameterization	N/A	N/A	N/A	N/A	4.52%	

Table A.5: TI Heavy Wind Light Load Cases: 2026_HWLL_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0	0	0.17	0.12	0.00%	
	P_{min} Exceedances	0	0.37	0	0	0.00%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Thermal Overloads	0.05	0.03	0.17	0.26	0.28%	
	Thermal Overloads (Severe)	0.04	0.01	0.13	0.24	0.24%	
	Low Emergency Rating	0	0	0	0	0.00%	
	High Emergency Rating	0.03	0	0.02	0.18	0.01%	
	Voltage Schedule Conflicts	12	62	43	79	117	
	Tap Step Conflicts	0	1.6	3.01	3.57	0.00%	
	Tap Step Conflicts (Severe)	0	0	0	0	0.00%	
	Generator Reactive at Limits	**12.59**	**14.01**	**9.16**	4.88	**13.19%**	
	Generator Reactive Limit Power Factor	**7.82**	**7.84**	**6.53**	**7.2**	**6.53%**	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.19	0.06	0.05	0.09	0.02%	
	Generator R_{source}:X_{source} Ratio	0.21	0	0.68	0.83	0.00%	
	X/R Ratio Check	0.43	0.43	0.34	0.42	0.37%	
	Generator Terminal Voltage	0	0	0.76	0.93	0.00%	
	Generator Reactive Capability Curve	0	0	0	0	0.00%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Generators without Models	**8.55**	2.93	3.08	1.79	3.65%	
	Generators with Classical Models	1.43	0	1.22	1.09	0.99%	
	Netted Gens with Models	0	0.38	0	0.41	0.00%	
	Netted Generators	0	0.38	0	0.41	0.00%	
	Inconsistent Reactances	1.23	1.07	1.31	1.13	1.47%	
	Unacceptable Models	2.79	2.11	1.85	1.42	1.98%	
	Not Recommended Models	**24.68**	**21.67**	**20.09**	**17.08**	**36.49%**	
	User-Written Models[1]	N/A	N/A	N/A	N/A	**15.47%**	

Table A.5: TI Heavy Wind Light Load Cases: 2026_HWLL_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	Inconsistent Time Constants	0.39	0.79	0.73	0.69	0.44%	
	Unreasonable Inertia Constants	**13.98**	**15.31**	**16.4**	**18.85**	**11.94%**	
	Unreasonable Saturation Factors	**13.19**	**12.85**	**13.55**	**13.12**	**12.69%**	
	Severe Saturation Factors	1.18	1.19	1.65	1.55	1.75%	
	PSS but no Excitation	0	0	0	0	0.08%	
	Inconsistent Speed Damping	3.07	2.82	2.91	2.92	0.87%	
	Inconsistent Lead-Lag Time Constant	0	0	0	0	0.00%	
	Erroneous Power Dev Fractions	0	0	2.44	**7.84**	**9.68%**	
	DC Exciter Self-Excitation Errors	**12.5**	**13.46**	**11.32**	**10.52**	**12.50%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**16.92**	**14.07**	**16.21**	**17.87**	**18.99%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	
	Second Generation Renewable Model Parameterization	N/A	N/A	0	0	4.57%	

Table A.6: TI Second Summer Peak Cases: 2029_SP_Final_NonCnv							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0	0	0.11	0	0.00%	
	P_{min} Exceedances	0	0	0	0	0.00%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Thermal Overloads	0.04	0.05	0.29	0.25	0.30%	
	Thermal Overloads (Severe)	0.04	0.04	0.25	0.23	0.21%	
	Low Emergency Rating	0	0	0	0	0.00%	
	High Emergency Rating	0.03	0	0.02	0.02	0.80%	
	Voltage Schedule Conflicts	23	37	39	37	-	
	Tap Step Conflicts	0.94	1.4	3.6	3.45	0.00%	
	Tap Step Conflicts (Severe)	0.8	0	0	0	0.00%	
	Generator Reactive at Limits	**9.14**	**16.28**	**13.37**	**20.91**	**17.09%**	
	Generator Reactive Limit Power Factor	**13.35**	**12.59**	**9.15**	**9.3**	**9.38%**	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	

Table A.6: TI Second Summer Peak Cases: 2029_SP_Final_NonCnv							
Type of Metric	**Metric**	**2019 Score (%)**	**2020 Score (%)**	**2021 Score (%)**	**2022 Score (%)**	**2023 Score (%**	**Performance**
	Poor Load Power Factor	0.13	0.04	0.02	0.05	0.00%	
	Generator R_{source}:X_{source} Ratio	0.13	0	0.43	0.61	0.00%	
	X/R Ratio Check	0.43	0.44	0.34	0.42	0.36%	
	Generator Terminal Voltage	0	0.3	0.29	0.67	0.00%	
	Generator Reactive Capability Curve	0	0	0	0	0.00%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	N/A	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	N/A	
Dynamics	Generators without Models	**5.19**	3.35	3.26	1.79	3.71%	
	Gens with Classical Models	1.43	0	1.21	1.09	0.98%	
	Netted Gens with Models	0	0.24	0	0.29	0.00%	
	Netted Generators	0	0.24	0	0.29	0.00%	
	Inconsistent Reactances	1.23	1.07	1.31	1.15	1.47%	
	Unacceptable Models	2.72	2.1	1.85	1.42	1.97%	
	Not Recommended Models	**24.57**	**21.76**	**20.09**	**16.79**	**36.34%**	
	User-Written Models[34]	N/A	-	-	-	**16.49%**	
	Inconsistent Time Constants	0.39	0.79	0.73	0.69	0.44%	
	Unreasonable Inertia Constants	**13.98**	**15.31**	**16.4**	**18.86**	**11.94%**	
	Unreasonable Saturation Factors	**13.21**	**12.85**	**13.55**	**13.13**	**12.69%**	
	Severe Saturation Factors	1.18	1.19	1.65	1.55	1.75%	
	PSS but no Excitation	0	0	0	0	0.08%	
	Inconsistent Speed Damping	3.07	2.82	2.91	2.92	0.87%	
	Inconsistent Lead-Lag Time Constant	0	0	0	0	0.00%	
	Erroneous Power Dev Fractions	0	0	2.44	**6.78**	**9.68%**	
	DC Exciter Self-Excitation Errors	**12.5**	**13.46**	**11.32**	**10.52**	**12.50%**	
	Inconsistent Type III Wind Speeds	0	0	0	0	0.00%	
	Suspect PSS2A/2B parameters	**16.92**	**14.07**	**16.21**	**20.38**	**19.05%**	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	
	Second Generation Renewable Model Parameterization	N/A	N/A	0	0	4.85%	

[34] Performance not tracked.

Western Interconnection

Table A.7: 2023 Heavy Summer Peak Case: 23HS4a							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0	0.23	0.28	0.37	0.31%	
	P_{min} Exceedances	0.03	0.32	0.21	0.26	0.37%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Voltage Schedule Conflicts	63	55	58	64	0.61%	
	Tap Step Conflicts	0.72	0.62	0.54	0.26	0.24%	
	Tap Step Conflicts (Severe)	0.45	0.05	0.07	0.06	0.02%	
	Low Emergency Rating	0.4	0.37	0.03	0.02	0.01%	
	High Emergency Rating	0.01	0.01	0.01	0	0.01%	
	Thermal Overloads	0.01	0.05	0.07	0.06	0.04%	
	Thermal Overloads (Severe)	0	0.04	0.05	0.04	0.01%	
	Generator Reactive at Limits	4.84	**5.5**	**5.19**	**6.65**	**5.52%**	
	Generator Reactive Limit Power Factor	**28.35**	**10.06**	**9.78**	**9.46**	**9.47%**	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.07	0.05	0.05	0.04	0.04%	
	Generator R_{source}:X_{source} Ratio	0.05	0.05	0.09	0.17	0.22%	
	Generator Terminal Voltage	3.9	**6.03**	**7.24**	**6.86**	**6.67%**	
	Generator Reactive Capability Curve	0	3.47	0	2.63	2.43%	
	X/R Ratio Check	0.18	0.19	0.19	1.38	0.21%	
	Natural Gas Generator Pmax	**72.3**	**84.13**	**79.67**	**75.74**	**77.10%**	
	Natural Gas Generator Pmax (Severe)	**5.94**	4.35	**6.41**	3.89	4.14%	
Dynamics	Generators without Models	4.89	**6.69**	**7.16**	**8.06**	**7.17%**	
	Netted Gens with Models	1.07	0.16	0.34	0.18	0.22%	
	Netted Generators	3.57	3.22	3.98	**5.03**	2.89%	
	Generators with Classical Models	0	0	0	0.00%	0.00%	
	Unacceptable Models	4.19	3.73	3.23	7.78%	2.59%	
	Not Recommended Models	**11.93**	**10.88**	**9.13**	**5.95%**	**6.70%**	

Table A.7: 2023 Heavy Summer Peak Case: 23HS4a							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
	User-Written Models[35]	N/A	-	-	0.01%	0.01%	
	Inconsistent Reactances	3.54	3.24	3.35	0%	3.54%	
	Inconsistent Time Constants	**5.87**	**5.74**	**6.16**	**6.33%**	**6.58%**	
	Unreasonable Inertia Constants	**13.06**	**11.9**	**11.69**	**10.25%**	**8.85%**	
	Unreasonable Saturation Factors	**19.74**	**19**	**19.14**	**16.92%**	**15.12%**	
	Severe Saturation Factors	**6.65**	**6.12**	**5.91**	**5.45%**	**5.34%**	
	PSS but no Excitation	0	0.72	0.76	1.98%	1.36%	
	Inconsistent Speed Damping	**7.22**	**7.24**	**7.04**	**6.74%**	**6.58%**	
	Inconsistent Lead-Lag Time Constant	2.49	2.48	3.11	**5.39%**	4.63%	
	Erroneous Power Dev Fractions	2.91	2.69	2.73	1.89%	3.57%	
	DC Exciter Self-Excitation Errors	4.98	**5.34**	**5.75**	**5.76%**	**6.11%**	
	Inconsistent Type III Wind Speeds	1.27	1.32	0	**0%**	0.00%	
	Suspect PSS2A/2B parameters	3.52	3.16	3.74	3.15%	2.83%	
	Second Generation Renewable Model Parameterization	N/A	N/A	**31.13**	**36.35%**	4.80%	

35 Performance not tracked.

Table A.8: WI Heavy Winter 2022–2023: 23HW3a1_22							
Type of Metric	Metric	2019 Score (%)	2020 Score (%)	2021 Score (%)	2022 Score (%)	2023 Score (%	Performance
Powerflow	P_{max} Exceedances	0.08	0.55	0.44	0.44	0.48%	
	P_{min} Exceedances	0.41	0.59	0.33	0.33	0.22%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Voltage Schedule Conflicts	63	54	64	64	0.66%	
	Tap Step Conflicts	0.61	0.57	0.34	-0.34	0.26%	
	Tap Step Conflicts (Severe)	0.06	0.06	0.08	-0.08	0.05%	
	Low Emergency Rating	0.14	0.35	0.35	-0.35	0.02%	
	High Emergency Rating	0.02	0.03	0.02	-0.02	0.01%	
	Thermal Overloads	0.01	0.02	0.04	-0.04	0.10%	
	Thermal Overloads (Severe)	0	0.02	0.01	-0.01	0.06%	
	Generator Reactive at Limits	3.81	4.69	**5.06**	**6.97**	**5.22%**	
	Generator Reactive Limit Power Factor	**27.41**	**10.28**	**9.58**	**9.58**	**8.71%**	
	Positive Sequence TX Circulating Current	0	0	0	0	0.00%	
	Poor Load Power Factor	0.06	0.13	0.04	0.04	0.10%	
	Generator R_{source}:X_{source} Ratio	0.16	0.11	0.2	0.2	0.23%	
	Generator Terminal Voltage	3.9	**6.18**	**10.15**	**10.15**	**6.80%**	
	Generator Reactive Capability Curve	0	3.37	0	2.56	0.35%	
	X/R Ratio Check	0.18	0.19	0.2	2.5	0.20%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	**97.61%**	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	1.14%	
Dynamics	Gens without Models	4.38	**8.26**	**7.87**	**7.87**	**7.53%**	
	Netted Gens with Models	0.4	0.2	0.23	0.23	0.05%	
	Netted Generators	2	2.93	3.3	3.3	2.91%	
	Generators with Classical Models	0	0	0	0	0.00%	
	Unacceptable Models (Total)	4.66	3.38	2.48	2.62	2.67%	
	Not Recommended Models (Total)	**12.36**	**10.18**	**6.59**	2.8	**6.93%**	
	User-Written Models[36]	N/A	-	-	0.3	0.01%	
	Inconsistent Reactances	3.32	3.52	3.45	0	3.53%	
	Inconsistent Time Constants	**6.02**	**6.15**	**6.49**	**7.87**	**6.55%**	
	Unreasonable Inertia Constants	**13.32**	**12.48**	**11.86**	**9.88**	**5.85%**	
	Unreasonable Saturation Factors	**19.75**	**19.85**	**19.13**	**16.66**	**11.77%**	

[36] Performance not tracked.

Table A.8: WI Heavy Winter 2022–2023: 23HW3a1_22							
Type of Metric	**Metric**	**2019 Score (%)**	**2020 Score (%)**	**2021 Score (%)**	**2022 Score (%)**	**2023 Score (%**	**Performance**
	Severe Saturation Factors	**6.7**	**6.39**	**5.83**	**5.61**	4.53%	
	PSS but no Excitation	0.11	0.66	0.98	2.62	1.07%	
	Inconsistent Speed Damping	**7.03**	**7.19**	**6.87**	2.8	**6.80%**	
	Inconsistent Lead-Lag Time Constant	2.59	2.39	3.27	3.27	3.04%	
	Erroneous Power Dev Fractions	2.86	3.26	2.69	2.69	3.64%	
	DC Exciter Self-Excitation Errors	**5.86**	**5.88**	**5.08**	**5.8**	**5.77%**	
	Inconsistent Type III Wind Speeds	0	1.52	0	**0**	0.00%	
	Suspect PSS2A/2B parameters	3.95	4.05	3.71	3.71	2.95%	
	Incorrect DER_A Tripping Parameters	0	0	0	0	0.00%	
	Second Generation Renewable Model Parameterization	N/A	N/A	**34.66**	**34.62**	**38.21%**	

Table A.9: WI Light Summer Cases 23LS1a							
Type of Metric	**Metric**	**2019 Score (%)**	**2020 Score (%)**	**2021 Score (%)**	**2022 Score (%)**	**2023 Score (%)**	**Performance**
Powerflow	P_{max} Exceedances	0.19	0.14	0.08	0.42	0.28%	
	P_{min} Exceedances	0.05	0.87	0.25	1.34	0.73%	
	Scheduled Interchange Sum	0	0	0	0	0.00%	
	Voltage Schedule Conflicts	62	56	58	0.61	0.63%	
	Tap Step Conflicts	0.45	0.6	0.53	0.33	0.26%	
	Tap Step Conflicts (Severe)	0.06	0.07	0.07	0.07	0.05%	
	Low Emergency Rating	0.39	0.37	0.03	0.12	0.01%	
	High Emergency Rating	0.02	0.01	0.01	0.01	0.01%	
	Thermal Overloads	0.01	0.01	0.04	0.05	0.02%	
	Thermal Overloads (Severe)	0	0.01	0.01	0.01	0.02%	
	Generator Reactive at Limits	**5.99**	**5.67**	**5.43**	**7.01**	3.76%	
	Generator Reactive Limit Power Factor	**28.43**	**10.6**	**9.94**	4.74	**9.32%**	
	Positive Sequence TX Circulating Current	0	0	0	**9.94**	0.00%	
	Poor Load Power Factor	0.06	0.08	0.08	0.06	0.07%	
	Generator R_{source}:X_{source} Ratio	0.05	0.05	0.09	0.22	0.22%	

Table A.9: WI Light Summer Cases 23LS1a							
Type of Metric	**Metric**	**2019 Score (%)**	**2020 Score (%)**	**2021 Score (%)**	**2022 Score (%)**	**2023 Score (%)**	**Performance**
	Generator Terminal Voltage	**7.3**	4.74	**5.2**	**6.77**	**5.29%**	
	Generator Reactive Capability Curve	0	2.18	0	2.39	0.00%	
	X/R Ratio Check	0.17	0.19	0.19	4.52	0.21%	
	Natural Gas Generator Pmax	N/A	N/A	N/A	N/A	**77.21%**	
	Natural Gas Generator Pmax (Severe)	N/A	N/A	N/A	N/A	4.12%	
Dynamics	Generators without Models	4.96	**6.84**	**7.3**	**8.46**	**7.19%**	
Dynamics	Netted Gens with Models	0.4	0.29	0.32	0.74	0.23%	
Dynamics	Netted Generators	2.94	2.83	3.46	6.08	2.84%	
Dynamics	Generators with Classical Models	0	0	0	0	0.00%	
Dynamics	Unacceptable Models	4.17	3.79	3.41	2.37	2.60%	
Dynamics	Not Recommended Models	**11.85**	**10.82**	**9.11**	2.48	**6.81%**	
Dynamics	User-Written Models[37]	N/A	-	-	0.21	0.01%	
Dynamics	Inconsistent Reactances	3.55	3.24	3.44		3.54%	
Dynamics	Inconsistent Time Constants	**5.88**	**5.74**	2.86	**6.33**	**6.64%**	
Dynamics	Unreasonable Inertia Constants	**13.01**	**12**	**10.95**	**9.84**	2.27%	
Dynamics	Unreasonable Saturation Factors	**19.72**	**19.39**	**13.57**	**19.96**	**11.73%**	
Dynamics	Severe Saturation Factors	**6.68**	**6.35**	1.67	**5.45**	4.44%	
Dynamics	PSS but no Excitation	0.28	0.55	0	0.54	0.98%	
Dynamics	Inconsistent Speed Damping	**7.19**	**7.24**	**10.12**	**6.74**	**6.55%**	
Dynamics	Inconsistent Lead-Lag Time Constant	2.48	2.47	3.55	3.47	4.62%	
Dynamics	Erroneous Power Dev Fractions	2.9	3.21	1.49	1.89	3.57%	
Dynamics	DC Exciter Self-Excitation Errors	**5.22**	**5.53**	**7.08**	5.76	**6.16%**	
Dynamics	Inconsistent Type III Wind Speeds	1.28	1.27	0	**0**	0.00%	
Dynamics	Suspect PSS2A/2B parameters	3.76	3.17	3.75	3.26	2.90%	
Dynamics	Second Generation Renewable Model Parameterization	N/A	N/A	**30.72**	**35.49**	**40.08%**	

[37] Performance not tracked.