

Industry Webinar

Modifications to PRC-025-1

August 16, 2017







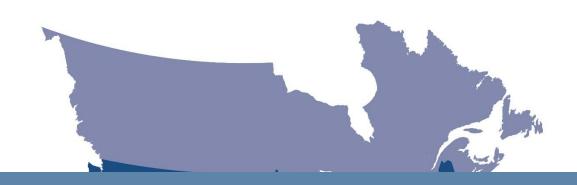
RELIABILITY | ACCOUNTABILITY





- Presenters
 - Standard Drafting Team
 - o Chair, John Schmall, ERCOT
 - o Vice Chair, Mike Jensen, PG&E
 - NERC Staff
 - Scott Barfield-McGinnis
- Administrative Items
- Background
- Revisions
- Q & A Session





Administrative Items





Antitrust Guidelines

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Public Disclaimer



Public Announcement

 Participants are reminded that this meeting is public. Notice of the meeting was widely distributed. Participants should keep in mind that the audience may include members of the press and representatives of various governmental authorities, in addition to the expected participation by industry stakeholders

Presentation Material

 Information used herein is used for presentation purposes and may not reflect the actual work of the official posted materials

For the official record

- This presentation is not a part of the official project record
- Comments must be submitted during the formal posting



Standard Drafting Team Roster

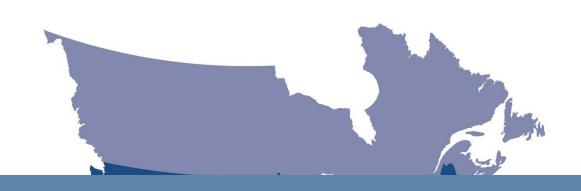
Member	Entity
John Schmall, Chair	Electric Reliability Council of Texas, Inc.
Mike Jensen, Vice Chair	Pacific Gas and Electric Company
Juan Alvarez	Caithness Energy
S. Bryan Burch, P.E.	Southern Company
Walter Campbell	NextEra Energy Resources, LLC
Jason Espinosa	Seminole Electric Cooperative, Inc.
Charles Yeung, PMOS Liaison	Southwest Power Pool, Inc.
Scott Barfield-McGinnis, PE	North American Electric Reliability Corporation
Lauren Perotti, Counsel	North American Electric Reliability Corporation

Q & A Objectives



- Informal discussion
 - Via the Q & A feature
 - Use chat speak with the host
 - Respond to stakeholder questions
- Help the team facilitate chat questions by
 - Prefacing comments with "Comment:"
 - Prefacing questions with "Question:
- Other
 - Some questions may require future team consideration
 - Please reference slide number, standard section, etc.
 - Team will address as many questions as possible
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 - Q&A recording will be posted within 48-72 hours





Background





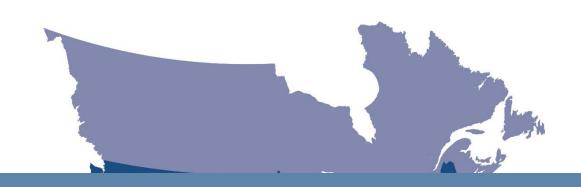
- Approval FERC Order No. 799 on July 17, 2014
- Effective on October 1, 2014
- Enforcement on October 1, 2019 (settings only)
- Enforcement on October 1, 2021 (Retire/Replace equipment)
- Issues revealed during implementation:
 - Need alternative loadability option(s)
 - 2. Address whether IEEE 50 device element is in or out
 - 3. Clarify Table 1 applications where there is more than one
 - 4. Need alternative option where the interconnecting transmission line impedance may be a factor
 - 5. Consider an alternative to the term "pickup setting"
 - 6. Clarify identified miscellaneous items





- Purpose statement
- Applicability
- Requirement
 - Except version reference
- Measure
- Violation Severity Levels





Revisions



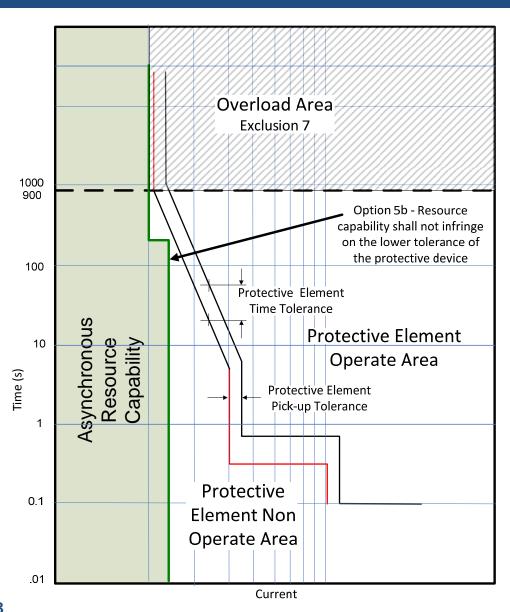


Alternative Loadability Option

Table 1. Relay Loadability Evaluation Criteria					
Application	Relay Type	Option	Bus Voltage ⁴	Pickup-Setting Criteria	
Asynchronous generating unit(s) (including inverter-based installations),	5 <u>a</u>	Generator bus voltage corresponding to 1.0 per unit of the high-side nominal voltage times the turns ratio of the generator step-up transformer	The overcurrent element shall be set greater than 130% of the calculated current derived from the maximum aggregate nameplate MVA output at rated power factor (including the Myar output of any static or dynamic reactive power devices)		
including or	overcurrent relay	<u>OR</u>	<u>OR</u>		
Elements utilized in the aggregation of dispersed power producing resources	(<u>e.g., 50, 51</u>) or (51V-R) – voltage- restrained)	<u>5b</u>	Generator bus voltage corresponding to 1.0 per unit of the high-side nominal voltage times the turns ratio of the generator step-up transformer	The protection element shall not infringe upon the resource capability (including the Myar output of any static or dynamic reactive power devices) with worst case documented tolerances applied between equipment capability and the protection element (see Figure A).	



Option 5b - Figure A



Setting Criteria

The protection element shall not infringe upon the resource capability (including the Myar output of any static or dynamic reactive power devices) with worst case documented tolerances applied between equipment capability and the protection element (see Figure A).



Address IEEE "50" Device Element

Table 1. Relay Loadability Evaluation Criteria			
Application	Relay Type	Option	Bus Volta
		2a	Generator bus voltage corresponding to 0.95 high-side nominal volta turns ratio of the gener transformer
		OR	
Synchronous generating unit(s),	Phase time overcurrent relay (e.g., 50, 51,) or (51V-R) – voltage- restrained)	2b	Calculated generator b corresponding to 0.85 nominal voltage on the terminals of the genera transformer (including transformer turns ratio impedance)



Clarify Table 1 Applications

Table 1. Relay Loadability Evaluation Criteria

Application	Relay Type	Option	
Asynchronous	Phase distance relay		G
generating unit(s)	(<u>e.g.,</u> 21) –		CO
(including inverter-	directional toward	4	hi
based installations),	the Transmission		tu
including or Elements	system		tr
utilized in the			
aggregation of			G
dispersed power			c
producing resources		Г-	
		5 <u>a</u>	hi
	Phase time		tu
	overcurrent relay		tr



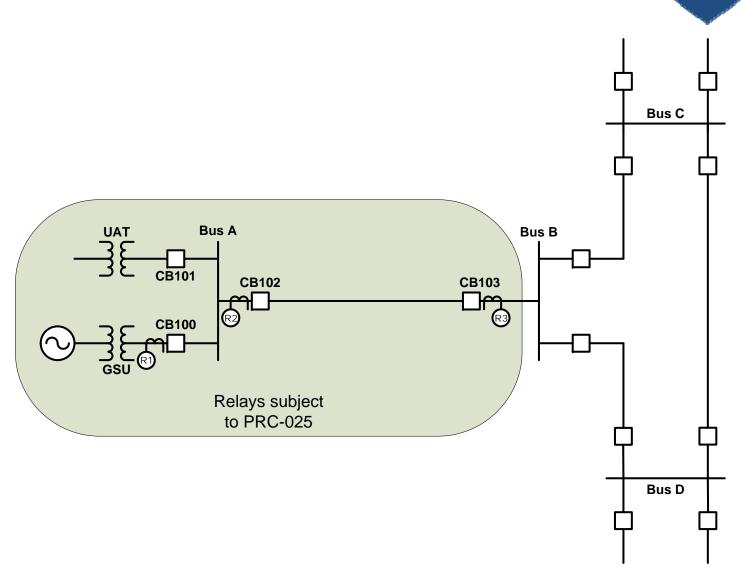


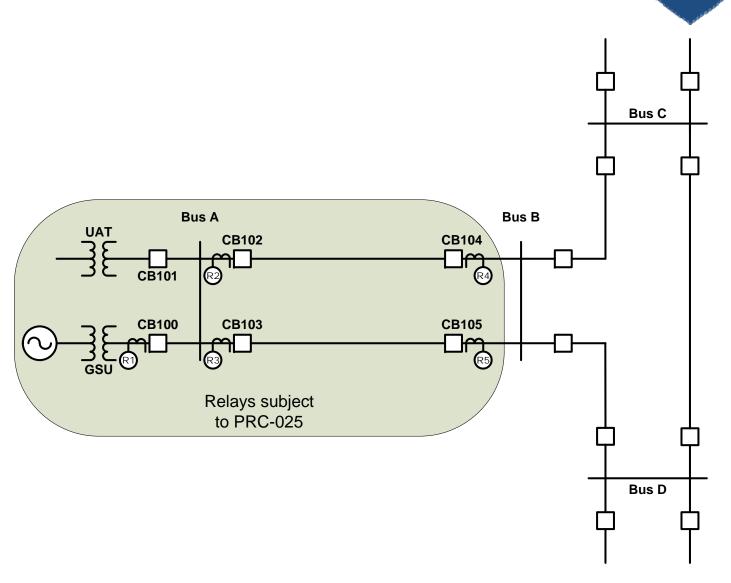
Plants Remote to Transmission

Lo	oadability·Evaluation·Criteria¤			
	Relay∙Type¤	Option¤	Bus∙Voltage∄¤	
å ±	Phase·distance·relay· (e.g.,·21)·—· directional·toward· the·Transmission· system·—·installed· on·the·high-side·of· the·GSU·	14a¤	0.85-per-unit-of-the-line-nominal- voltage-at-the-relay-location¤	The impedan (1) Real i MW repo (2) React MW valu at rated
	transformer <u>andon</u>	ORX		
t·	the·remote·end·of· line ^{fili} ¶ If-the·relay·is· installed·on·the· generator-side·of· the·GSU· transformer·use· Option·7¤	14b¤	Simulated·line·voltage·coincident· with·the·highest·Reactive·Power· output·achieved·during·field-forcing· in·response·to·a·0.85·per·unit· nominal·voltage·on·the·high-side· terminals·of·the·generator·step-up· transformerat·the·remote·end·of·the· line·prior·to·field-forcing¤	The·impe impedan (1)·Real·l MW·repo (2)·React maximur by·simula













ige ⁴	Pickup -Setting Criteria
per unit of the age times the rator step-up	The impedance element shall be set less than the calculated impedance derived from 115% of: (1) Real Power output – 100% of the gross MW capability reported to the Transmission Planner, and (2) Reactive Power output – 150% of the MW value, derived from the generator nameplate MVA rating at rated power factor



Miscellaneous Clarifications

- IEEE C37.17-2012 & IEEE C37.2-2008
- Asynchronous Generator Performance
 - Asynchronous generators, however, do not have excitation systems and will not respond to a disturbance with the same magnitude of apparent power that a synchronous generator will respond.
- Synchronous generator...
 - ...the maximum capability shall be used for the purposes of this standard as a minimum requirement. The Generator Owner may base settings on a capability that is higher than what is reported to the Transmission Planner.
- Asynchronous generator...
 - If different seasonal capabilities are reported, the maximum capability shall be used for the purposes of this standard as a minimum requirement. The Generator Owner may base settings on a capability that is higher than what is reported to the Transmission Planner.





Questions and Answers



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- Initial comment period
 - 45-Days
 - Initial Ballot (August 29 September 7, 2017)
- Respond to Comments
 - Meeting at Atlanta, GA| September 26-28, 2017
- Point of contact:
 - Scott Barfield-McGinnis, Senior Standard Developer
 - o <u>Scott.Barfield@nerc.net</u> or call 404-446-9689
- Webinar posting

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Within 48-72 hours



Industry Webinar Has Ended

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Point of contact: Scott Barfield-McGinnis, Senior Standards Developer or call 404-446-9689

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